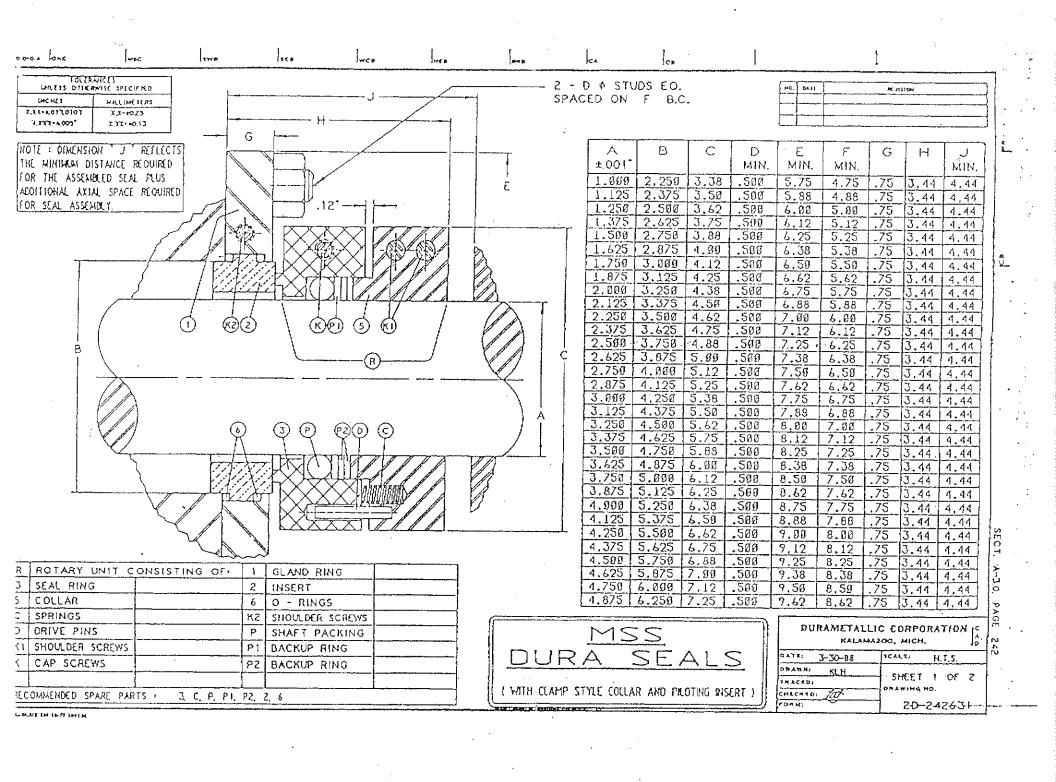
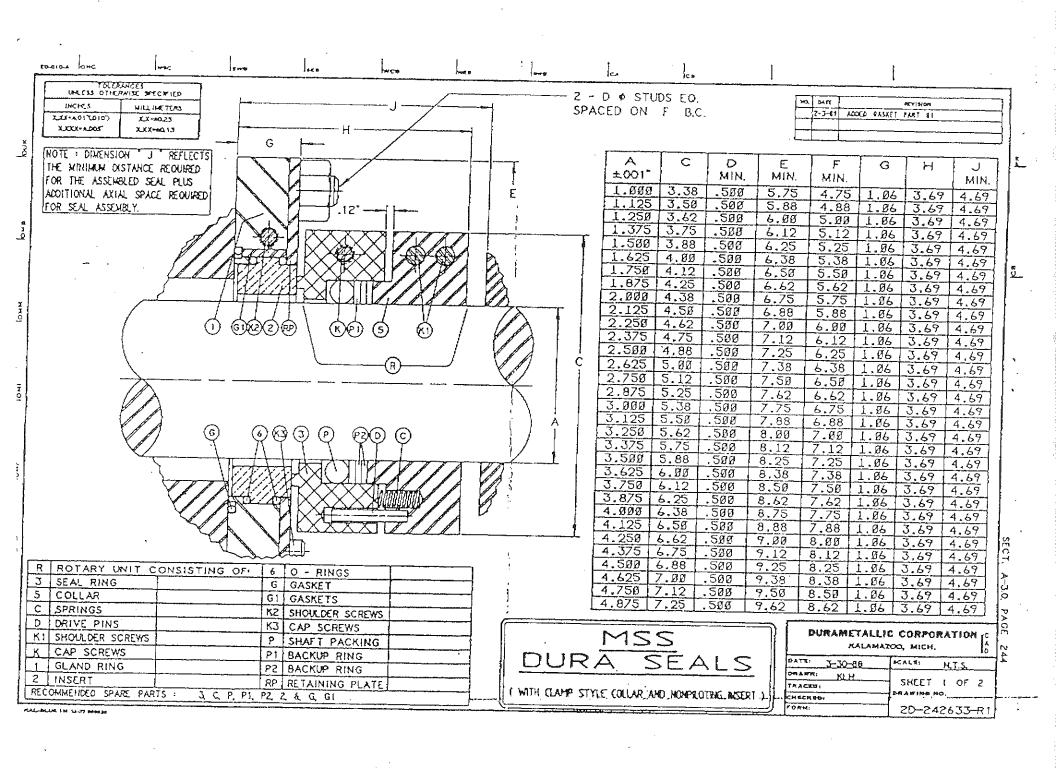
## Section 11001

## Miscellaneous Equipment

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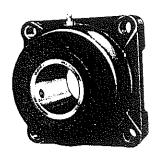


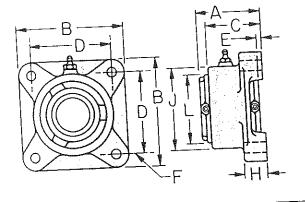
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NON-EXPANSION TYPE



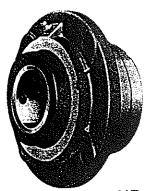


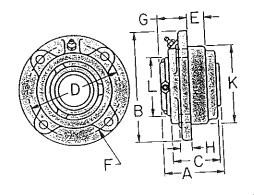
#### MODEL EFB4

MODEL EFB4				D	MENSION	s		<u> </u>		Wt.	
Shaft					Е	F	н	J	L	Lbs.	
Shart Size 1½, 1½ 1½, 1½, 1½, 1½, 11,6 1½, 1½, 11,6 2,2	213/16 31/16 31/2 35/8 37/8	3¾ 4½ 5⅓ 5⅓ 6¼	211/32 219/32 231/32 33/32 34/32 34/36	D 27/6 3 ½ 4 ½ 4 ¾ 4 ¾ 5 ¾	1/16 1/16 1/16 1/16 1/16	80lt % ½ ½ ½ ½ ½ %	1 1 1/16 1 1/16 1 1/16 1 1/2	215/16 31/2 43/16 47/16 47/6 55/16 6	2¼ 2¾ 3¾6 3¼6 3¾ 4 4¼6 4²¾32	4.4 6.8 11.1 11.7 15.5 20.6 26.9	
24, 276, 24 2146, 24, 2146, 3 346, 34, 376, 34	4 <sup>3</sup> / <sub>16</sub> 4 <sup>1</sup> / <sub>1</sub> / <sub>6</sub> 5 <sup>1</sup> / <sub>4</sub> 6 <sup>1</sup> / <sub>2</sub>	6% 7% 9% 10%	315/16 41/4 55/8	6 7 74	¥16 V4 V4	√4 √4 √8	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7¼ 8¼	5½6 5½6	51.3 75.1	

<sup>†</sup>Assembled to order. Consult factory for delivery.

## NON-EXPANSION TYPE





## MODELS EFC4 AND EFC6

											STATE OF THE OWNERS	Ling to be part in
ļ	MODELS EFC	1 AND	<u>EFC6</u>	FARRY -		DIMEN	SIONS 🥌	<b>米尔·</b> 尔德	150 St. 5150			Wt
	Shaft Shaft			;;/(≥ 1= C	D	<b>E</b>	F Bolt	G	H	+.000 002	L	Lbs.
	Size	A	Sale See See See See See See		4⅓	9 <sub>4</sub>	% □□□□⊕₩₩	15/16	1/16	3% 3%	2¼ 2¾	5.1 6.4
	1 <sup>3</sup> / <sub>16</sub> , 1 <sup>1</sup> / <sub>4</sub> 1 <sup>3</sup> / <sub>8</sub> , 1 <sup>3</sup> / <sub>16</sub>	2¾ 3	5 5¼	2 <sup>7</sup> / <sub>32</sub> 2 <sup>1</sup> / <sub>32</sub> 2 <sup>2</sup> / <sub>32</sub>	4% 4% 5%	1½ 1½	⅓ <sub>8</sub> 7/₁6	1½ 1%	1/2 1/2 9/16	41/4 41/2	37/16 37/16	9.4 10.6
	1½, 1‰, 1¼6 1¾, 1‰, 1¼6, 2	3% 3½ 3¾	6% 6% 7%	2 <sup>29</sup> / <sub>32</sub> 3 <sup>3</sup> / <sub>32</sub>	5¾ 6	13/16 13/16	/ <sup>1</sup> / <sub>16</sub>	1%6 11%6	9/16	5	3¾	13.6
	27/16	1 374	75/8	35/16	61/2	1 1/2	1/ <sub>2</sub> 5/8	11 <del>7</del> 16 2	5% 3√4	5½ 6%	41/16 4 <sup>2</sup> / <sub>32</sub> 5 <sup>7</sup> / <sub>16</sub>	25.8 42.8
	24, 21/6, 21/2 211/6, 23/4, 21/4, 3 34/6†, 31/4†, 31/6, 31/2†	4½ 5	8¾ 10¼	311/16 43/16	7½ 8% 9%	11/2	¥, ¥,	2 <sup>7</sup> /16 2 <sup>1</sup> //16	7/8 15/16	7% 8% 10%	515/16	57.4 92.5
	315/16, 4† 47/16, 4½†	6¼ 6¾	10%	4½ 4½ 5½	1111/4	11/2	¾; %‡	31/32 231/32	11/4	1 11	7½	as shown in
	415/ C+	7 1/4	147/4_	1 2/16	_1			Ciron 13	31/4 rise s	indie lock	my condi	

<sup>†</sup> Assembled to order. Consult factory for delivery. 

14 equally spaced unless otherwise noted. 

16 equally spaced.

Note: Sizes 11/16-31/2 use single locking collar as shown it drawing.



#### HUB CITY BEARING UNITS

Heavy Service — For heavy shock loads, frequent shock loads, or severe vibrations, add up to 50% (according to severity of conditions) to the Equivalent Radial Load to obtain a Modified Equivalent Radial Load. Consult customer service for additional selection assistance.

Select a bearing from the rating table having a radial load rating at the operating speed equal to or greater than the calculated "Equivalent Radial Load" for a desired L10 Life. This simple method is all that is required for the majority of general machine applications and provides for occasional average shock loads.

To determine the L10 Hours Life for loads and speeds not listed, use the following equation:

L10 = 
$$\left(\frac{\text{C90}}{\text{P}}\right)^{10/3} \times \frac{1,500,000}{\text{RPM}}$$

Where:

C90 = Dynamic Capacity (Table 1)
P = Equivalent Radial Load, Lbs.

When the load on a two row roller bearing is solely a radial load with no thrust load, the load is shared equally by both rows of rollers and the equivalent radial load (P) is equal to the actual radial load. However, when a thrust load is applied, the loading on the two rows is shared unequally depending on the ratio of thrust to radial load. The use of the X (radial factor) and Y (thrust factor) from Table 1 convert the actual applied loads to an equivalent radial

load having the same affect on the life of a bearing as a radial load of this magnitude.

The equivalent radial load P = X Fr + Y Fa

If calculated value of P is less than Fr, then use P = Fr

Where P = Equivalent radial load, lbs.

Fr = Radial Load, lbs.

Fa = Thrust (axial) load, lbs.

e = Thrust load to radial load factor (Table 1 below)

X = Radial load factor (Table 1 below)

Y = Thrust load factor (Table 1 below)

To find X and Y, first calculate Fa/Fr and compare to e. Determine X and Y from Table 1: Light thrust if Fa/Fr is less than or equal to e or heavy thrust if Fa/Fr is greater than e.

Substitute all known values into the equivalent radial load equation. P (equivalent radial load) thus determined can be used in life formula to determine L10 or compared to allowable equivalent radial load ratings for the speed and hours life desired in rating table.

L10 Hours Life — Is the life which may be expected from at least 90% of a given group of bearings operating under identical conditions.

1ACC

:46)

TABLE 1

Shaft Size	e -	Thi	国际设置	He Thi 沙沙汀 华Fa/F	uste I	C	ynamic apacity C90.*	Maximum a	Maximum Siit Ett Hadiai
		it-Xibit	\$3.5 Y \ 1.75	· X (2.5	4 Y **	Lbs	Newtons @		Load France
1 / 1/4	.49	.87	1.77	.70	2,14	2,980	13,260	4,490	5,600
13/6-17/16	.46	.87	1.89	.70	2.28	4,760	21,180	3,820	5,600
1 1/2-1 1 1/16	.44	.87	1.96	.70	2.37	6,140	27,320	3,320	5,600
1¾-2	.33	.87	2.64	.70	3.18	8,070	35,908	3,050	8,210
2¾6	.36	.87	2.38	.70	2.87	8,550	38,044	2,730	8,210
21/4-21/2	.40	.87	2.17	.70	2.63	9,090	40,447	2,420	8,210
211/46-3	.46	.87	1.87	.70	2.26	9,600	42,716	2,060	13,800
3¾15-31/2	.50	.87	1.71	.70	2.07	15,300	68,078	1,640	13,800
315/16-4	.49	.87	1.77	.70	2.14	21,000	93,440	1,530	22,000
41/16-41/2	.53	.87	1.63	.70	1.97	25,800	114,799	1,360	32,500
415/16-5	.47	.87	1.83	.70	2.21	35,500	157,959	1,200	32,500
5%6-6	.49	.87	1.76	.70	2.12	40,700	181,097	915	53,000
61/16-7	.54	.87	1.61	.70	1.95	69,200	307,910	790	100.000

<sup>\*</sup> C90 — Dynamic capacity based on a rated life of 90 million revolutions or 3,000 hours at 500 RPM.

#### COMPARING SPHERICAL TO TAPER ROLLER BEARING

The dynamic capacity C (spherical) and C90 (taper) are not to the same base. To compare basic dynamic capacities, multiply C × .259 and compare to C90. To select and then compare, use the complete selection procedure for each type bearing and then compare.

<sup>\*\*</sup>If load exceeds maximum allowable slip fit radial load, snug to light press fit of shaft is required.

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61/2

7

615/16

10,000

30,000

50,000

100,000

155930 118450

112150

96210

78150

85200

73090

59370

Shaft	L10 Life		1	llowable	Equival	ent Rac	100 (50, 150)									haaa	T	
Size	Hours	.∡10	25	50	100 👵	150 🎋			1 -3	** ** * ** *** ****	***	1500 >		1	17 207 - 5	3000	1	
	5,000	8270	6280	5100	4145	3670	3145 2555	2555 2075	2265 1840	2075 1685	1940 1575		1755 1425	1685 1370	1575 1280	1495 1215	1425 1160	
13/16	10,000 30,000	6720 4830	5100 3670	4145 2980	3365 2420	2980 2145	1840	1495	1320	1215	1135		1025	985	920	870	835	
11/4	50,000	4140	3150	2555	2075	1840	1575	1280	1135	1040	975	920	880	845	790	750	715	
	100,000	3360	2550	2075	1685	1495	1280	1040	920	845	790	750	715	685	640	610	580	
	5,000	13210	10030	8150	6620	5860	5025	4085	3615 2935	3315 2695	3100 2520		2805 2275	2695 2190	2520 2045	2385 1935	2275 1850	ĺ
1 7/8	10,000	10730 7710	8150 5860	6620 4 <b>760</b>	5375 3865	4760 <b>3425</b>	4085 2935	3315 2385	2110	1935	1810	1715	1640	1575	1470	1395	1330	
11/16	50,000	6620	5030	4085	3315	2935	2520	2045	1810	1660	1555	1470	1405	1350	1260	1195	1140	ĺ
	100,000	5370	4080	3315	2695	2385	2045	1660	1470	1350	1260	1195	1140	1095	1025	970	925	į
	5,000	17030	12940	10510	8535	7560	6485	5265	4665	4280	4000 3250	3790 3075	3615 2940	3475 2820	3250 2640	3075 2500		
11/2	10,000	13830	10510	8535 <b>6140</b>	6935 <b>4985</b>	6140 <b>4415</b>	5265 <b>3790</b>	4280 <b>3075</b>	3790 <b>2725</b>	3475 2500	2335	2215	2115	2030	1900	1795		
1% : 1¹⅓s	<b>30,000</b> 50,000	<b>9950</b> 8530	<b>7560</b> 6480	5265	4280	3790	3250	2640	2335	2145	2005	1900	1810	1740	1630	1540		
' ''	100,000	6940	5270	4280	3475	3075	2640	2145	1900	1740	1630	1540	1470	1415	1325	1250	-	
13/	5,000	22390	17010	13815	11220	9935	8525	6925	6130	5625	5260	4980	4755	4565 3710	4270 3470	4045 3285		
11/4	10,000	18180	13810	11220	9115	8070 5805	6925 4980	5625 4045	4980 3580	4565 3285	4270 3070	4045 2910	3860 2775	2670		2360		
115/16	30,000 50,000	13080	9940 8530	8070 6925	6555 5625	4980	4270	3470	3070	2820	2635	2495	2380	2290	2140	2025		
2 -	100,000	9120	6930	5625	4565	4045	3470	2820	2495	2290	2140	2025	1935					
	5,000	23720	18020	14635	11885	10525	9030	7335	6495	5960	5570	5275	5035 4090					
	10,000	19260	14630	11885	9655	8550	7335	5960 4285	5275 3795	4840 3480	4525 3255	4285 3080	1	- I		1		
23/16	50,000	13860 11890	1 <b>0530</b> 9030	8550 7335	6945 5960	6150 5275	5275 4525	3675	3255	2985	2790	2645						
	100,000	9660	7340	5960	4840	4285	3675	2985	2645	2425	2270	2145	2050	1970	1840			
	5,000	25220	19160	15560	12640	11190	9600	7800	5905	6335	5925	5610	1			- 1		
21/4	10,000	20490	15560	12640	10265	9090	7800	6335	5610 4035	5145 3700	4810 3460	4555 3275				í		
2/16	30,000	14730 12640	11190	9090 7800	7385 6335	6535 5610	5610 4810	4555 3910	3460	1	2970	2810		1				
21/2	50,000	1	7800	6335	5145	4555	3910	3175	2810		2410	2285		2095	1960			
211/	5,000		20230	16430	13345	11820	10140	8235	7290		6255	5925						
211/16	10,000		16430	13345	10840	9600	8235	6690 4810	5925 4260		5080 3655	4810 3460	1					
215/16	30,000 50,000		11820	9600 8235	7795 6690	6905 5925	5925 5080	4125	3655	3	1			1				
3	100,000		8240	6690	5435	4810	4125	3350	2970		2545	2410	2300	0 2210	)			
23/	5,000	42440	32240	26190	21270	18835	16160	13125				1						
31/4	10,000		26190	21270	17280	15300	13125	10660 <b>7670</b>			,	1	1					
31/16	30,000 50,000		18840	15300	1	11005 9440	9440 8100	6580				ì						
31/2	100,000	1	13120	1			1	1				384	5_					
	5,000	58250	44250								1							
315/16	10,000				23715		18015				5   11115 799!							
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	100,000				11885	10525					5 5570	527	5_]					
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415/16	10,00	0   80000	60770		40090													
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	100,00					5 1779	1526		0 1098	0 1007	F							
	5,00			<del></del>	0 56590	5010	5 42990	3491							1			
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515/16						0 <b>2927</b> 0 2511						: - :	- ANI	M. IMI	オスロコリ	4111	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	•
6	50,00			0 2836	0 2303								~~~~	70	1111155	1 D V I		1
	5.00		0 14584	0 11845	5 9621	5 8519	5 7309	0 5936	5 5257	70			~ ^ + h	ar co	HIBLIO,	110111		c
67/16		0 155930		0 9621	5 7815	0   6920	0  5936	5   4822	0 4270	00	1000	igth Oi	-40 t	hrou	gh K	42.	teter	ţ

igs of dial or strength or other components. Refer to pages K-40 through K-42. Refer to Table 1, page K-42 for maximum RPM and maximum slip filt radial load.

25345

96215 | 78150 | 69200 | 59365 | 48220 | 42700

69200 | 56205 | 49770 | 42700 | 34680 | 30710

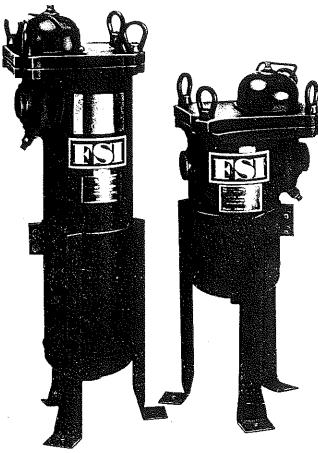
48220 39170 34680 29755 24170 21400

59365 | 48220 | 42700 | 36630 | 29755

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## SINGLE BAG FILTER VESSELS



Model FSP-85 Style 1

Model FSP-40 Style 4

#### MODEL FSP-48

Features up to 4" full port that permits non-restricted flow. Straight in-line design available. Makes manifolding easy. New basket design eliminates need for gaskets. Designed for continuous flow up to 100 GPM and small-batch operations. Requires one size #1 filter bag.

#### MODEL FSP-85

Features up to 4" full port that permits unrestricted flow. Straight in-line design available. Makes manifolding easy. New basket design eliminates need for gaskets. Designed for continuous flow up to 200 GPM and batch operations where Model FSP-40 does not have the capacity. Requires only one size #2 filter bag.

#### STYLES

The new models FSP-40 and FSP-85 are available in styles shown on the opposite side of this page.

#### TYPICAL APPLICATIONS

Typical applications for both the FSP-40 and FSP-85 include paints, chemicals, inks, coatings, resins, solvents and adhesives.

#### FILTER BAGS VS. CONVENTIONAL CARTRIDGES

Model FSP-40: Performance of the FSP-40 is equal to approximately six to nine (6-9) conventional 10" cartridges.

Model FSP-85: Performance of the FSP-85 is equal to approximately twelve to eighteen (12-18) conventional 10" cartridges.

#### **SPECIFICATIONS**

Model No.	No. of Filter Bags	Bag Size No.	Surface area Per bag, ft. <sup>2</sup>	Surface area per filter, ft²	Inlet and Outlet Size	Max. flow rate, GPM
FSP-40	- <b>1</b>	1	2.0	2.0	1" thru 4"	90
FSP-85	1	2	4.4	4.4	1" thru 4"	200

Maximum flow rate is based on aqueous flow at 1.0 PSI  $\triangle$ P clean through vessel only without bags installed.

#### **ADDITIONAL FEATURES**

- Single gasket seal
- · Positive bag sealing
- · Easy access for fast cleaning
- · Permanent piping
- Heavy-duty baskets (standard)
- New float evacuation system (optional)
- Can be supplied with steam jackets, extralength legs and corrosion allowance
- Mesh lined baskets available for straining applications
- Data obtained using the FSP-40 or FSP-85 filters can be extrapolated to estimate the performance of larger FSI filters

#### SPECIFICATIONS

- Standard 2" inlet & outlet
- Specific locations and sizes up to 4" available on request
- 4 standard styles
- Stock vessels available in:
  - 1. Carbon steel
  - 2. 304 stainless steel
- 316 stainless steel and electroless nickel plated carbon steel vessels available on request
- Standard 150 or 300 PSI ASME code stamp (meets OSHA requirements) or customer specification
- Filter bags available rated 1 to 1500 microns
- Gasket materials include Buna N, Neoprene, EPR, Viton, Teflon

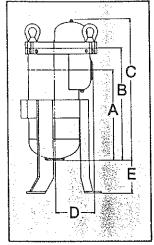
There are no expressed or implied warranties, including the implied warranty of merchantability and fitness for a particular purpose not specific herein respecting this agreement or the product being sold hereunder or the service provided herein.

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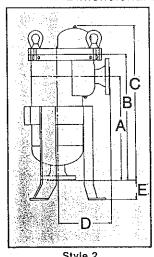
## mensions nominal, not to be installation purposes not to be used for

#### **STYLES**

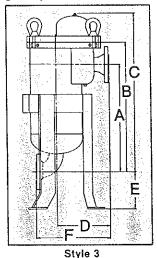
Styles one thru four (1-4) are shown below (available for both the FSP-40 and FSP-85). Dimensional drawings, styles 1, 2, 3 & 4



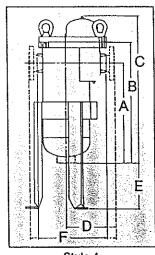
Style 1 (2" NPT Fittings)



Style 2 (2" Flanged Fittings)



(2" Flanged Fittings with 90° Elbow)

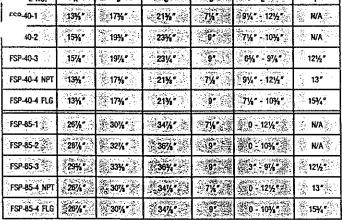


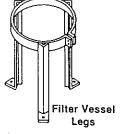
Style 4 Inline 2" NPT or Flanged

#### FSP-40 and FSP-85 dimensions

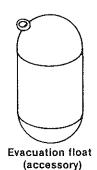
L XO.	(A) A ( )	<b>%</b> ∈8	₩C.	- AD ¥®	·黎斯·西波尔·	* <b>F</b>
ECD-40-1	13%*	17%*	21%"	7/4	914" - 1214"	₹ WAS-
40-2	15%*	19%"	23%	9.	7%" - 10%"	* N/A
FSP-40-3	15%"	197/1°	231/4"	9.	6%* - 9%*	121/2"
FSP-40-4 NPT	13%*	17%*	21%*	7%"	914" - 1214"	13"
FSP-40-4 FLG	13%"	17%"	21%"	97	7%" - 10%"	15¾"
FSP-85-1	267/6"	<b>₹</b> 30%*}	347/6"	7%"	€ 0 - 12½°	ş N/A}
FSP-85-2	287%*	≥:.32¼°≟	36%	9.	0 - 10%*	Ş NA ₹
FSP-85-3	29%	33%	36%	97	31 9/6	121/2
FSP-85-4 NPT	267/,*	307/17	34%	-27 <b>7</b> 7	©0 - 121/4° ⊅	🤹 13 <b>*</b>
FSP-85-4 FLG	±26%*.	₹ 30%	%34%°.∞	. 9.	<b>* 0 - 10%</b> *	ी 15५/₄*ं

Dimensions shown are for 2" littings.

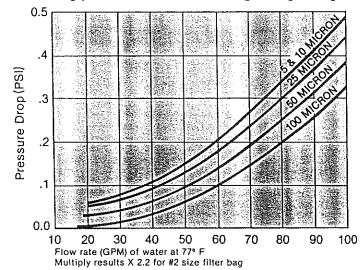




Heavy-duty restrainer basket



Filter bag performance data for single-length bags



Note 1: For recommendations on which bag or filter housing material to use, and for complete technical data or pressure drop and flow rate - also how to size FSI bag filters - contact your FSI representative or FSI direct.

Note 2: 2" NPT drain standard on style 4 vessels.

Note 3: Customer to specify plping size and type connections if different from standard 2".



Tilltær spæciallists, imc.

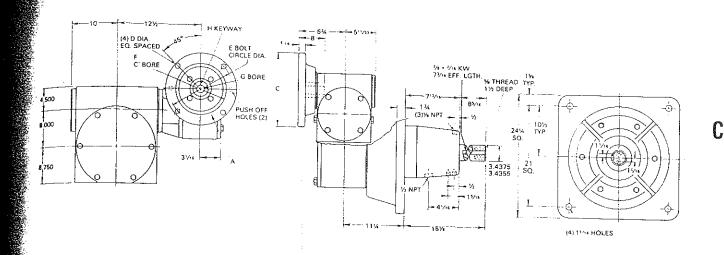
100 Anchor Road P.O. Box 735 Michigan City, Indiana 46360 219/879-3307

Dis	tri	but	ad	hv:

		C.
		· · ·
		1.0
		TN English
		*
		• •

## HUB CITY DOUBLE REDUCTION WORM GEAR REDUCERS

## Series 80D, Model 8008



NEMA Flange a	В	C		B.C. DIA. E	COUNTER BORE	MOTOR SHAFT QUILL	KEYWAY	KEY Furn- Ished
56C	2¾	6%	13/32	51/4	4.501 4.503	.6255 .6270	11 3√1.5 × 3√3.2	-⊁₄Sq.
143TC, 145TC, 182C, 184C	2%	6%	13/12	5%	4.501 4.503	.8755 .8770	¥6 × ₹52	⊁ւ Sq.
182TC, 184TC, 213C, 215C	3₹15	9	17/32	7¼	8.501 8.504	1.1255 1.1270	¼ × ⅓	1/4 Sq.
213TC, 215TC	31/2	9	17/32	7¼	8.501 8.504	1.3755 1.3770	%6 × ⅓2	%∈Sq.

MOI	DELS
PRIMARY	SECONDARY
454	807

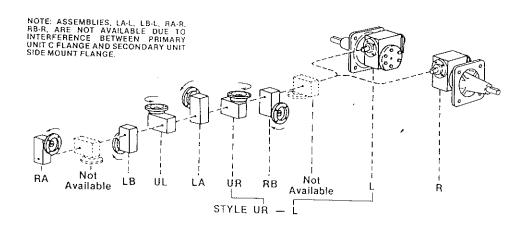
FACTORY ASSEMBLED ONLY.

HUB CITY LUBRICANT RECOMMENDED. (REFER TO PAGE L-20.)

DIMENSIONS SHOWN ARE FOR REFERENCE ONLY. CERTIFIED PRINTS ARE AVAILABLE UPON REQUEST.

DRY SHIPPING WEIGHT 991 LBS.

### STANDARD STYLES AVAILABLE



INPUT SHAFT CAN BE ROTATED IN EITHER DIRECTION



## HUB CITY DOUBLE REDUCTION WORM GEAR REDUCERS

## Series 80D, Ratings

3600

				NSEC	HANIC	AL R	ATINO						ТНІ	ERMAI	_ R/	ATING
			1	183 F- C				ACTOF				EI-	t	ESIGN	OPT	TION
R A		Ra	1	1.0	n	1.2		1.5		1.7	75	ti- cien-	Ba	sic Unit	Synt	With thetic Lube
ĭ	Output	Pri-	Sec-	Input	Output	input (	Dutput Forque		Output Torque	Input H.P.	Output Torque	су %	Inpu H.P.	Oulput Torque		
0	R.P.M.	mary	175			PUT		EED	HIG	H SP	EED S	HAFT)	)			
			· · · · ·				35926	10.87	29939	9.31	25662	76.5	7.55	20800	8.5	8 23920
100	17.5	10	10	16.3 12.4	44908 47895		38316	8.27	31930	7.09	27369	71.5	5.35	20670	6.1	1
150	11.7 8,75	15 10	10 20	10.4	52384	8.32	41907	6.93	34923	5.94	29934	69.9	7.55	38010	B.6	8 43710
200	8,73	10									0.4507	65.0	5.35	37570	1 6.1	5 43210
300	5.83	15	20	7.87	55295	6.30	44236	5.25 4.15	36863 37398	4.50 3.55	31597 32055	62.6	4.53		5.2	
400	4.38	20	20	6.22	56097 51217	4.98 4.10	44878 40974	3.41	34145	2.93	29267	55.5	4.36	43590	5.0	50130
500	3.50	10	50	5.12	31217	4.10	40011	•		i					1	ļ
-00	2.92	15	40	5.00	58451	4.00	46761	3.33	38967	2.86	33401	54.1	3.81		1	тои
600 750	2.33	15	50	3.81	52325	3.05	41860	2.54	34883	2.18	29900 29900	50.8	3.02			
1000	1.75	20	50	3.02	52325	2.42	41860	2.01	34883	1.73	29900	70.1	"			EQUIRED
			10	3.02	56644	2.42	45315	2.01	37763	1.73	32368	43.4	3.0			
1200	1.46	30 50	40 30	2.50	55257	2.00	45206	1.67	36838	1.43	31575	40.9	2.30			50 55257
1500 1800	1.17	60	30	2.21	55257	1.77	45206	1.47	36838	1.26	31575	38.6	2.0	7 5180	2.	21 55257
1800	1 312								07000	1.15	31914	38.3	2.0	2 5584	9	иот
2000	.875	50	40	2.02	55849	1.62	44679	1.35 1.20	37233 37233	1.15	31914	36.0	1.8			
2400	,729	60	40	1.80	55849	1.44 1.20	44679 43303	1.00	36086	.857	30931	33.4	1.5	0 5412	9 R	EQUIRED
3000	.583	60	50 60	1.50	54129 41905	,832	33524	.693	27937	.594	23946	31.1	1.0	4 4190	5	
3600	.486	60		·	1		T 01	PEEC	3 /111		PEED	CHVE.	_ \ T\			
			115	UKI	M II	APU.	·	Τ		. ]	29130	76.8	6.1	8 2601	0 7	.11 29910
100	11.5	10	10	12.1	50977	9.68	40782	8.07	33985 34487	6.91 4.97	29130	72.3	4.4	-	1	3,14 30560
150	7.67	15	10	8.70	51730	6.96	41384 45965	5.80 5.01	38305	4.29	32833	69.8	6.	8 4728	SO 7	1.11 54370
200	5.75	10	20	7.51	57457	6.01	45900	3.01	50000			ļ	1 1		ļ	
	200	15	20	5.25	56097	4.20	44878	3.50	37398	3.00	32055	65.0	4.4			5.14 54940
300 400	3.83	20	20	4.08	56097	3.26	44878	2.72	37398	2.33	32055	62.7	3.1		1	1.08 56097
500	2.30	10	50	3.50	52325	2.80	41860	2.33	34883	2.00	29900	54.6	3.	50 525	23	
								2.13	37233	1.82	31914	53.3	3.	19 558	49	
600	1,92	15	40	3.19	55849	2.55 2.05	44679 41860	1.71	34883	1.46	29900	49.8	2.	56 <b>523</b>	25	
750	1.53	15 20	50 50	2.5 <del>6</del> 2.02	52325 52325	1.62	41860	1.35	34883	1.15	29900	47.3	2.	02 523	25	NOT
1000	1.15	20	30	2.02	52020	,,				1		45.6	11.	95 558	40	NOT
1200	.958	30	40	1.95	55849	1.56	44679	1.30	37233	1.11	31914	43.6	1 1	95 550 63 552		REQUIRED
1500	.767	50	30	1.63	55257	1.30	44206	1.09	36838 38571	.931		39.1	1 1 '	50 578		
1800	.639	60	30	1.50	57857	1.20	44206	1.00	3037 L	.03/	5,0001	1				
2000		5 50	40	1,32	55849	1.06	44679	.880	37233				1 1	.32 558		
2000	,575 ,479	i i	40	1.16	55849	.928	44679	.773				t		.16 558 .944 520		
3000	.380	1	50	.944	52325	.755	41860	.629		1					005	
3600	.319	9 60	60	.676	41905	.541	33524	.45								
			85	0 RI	M II	NPU	T SI	PEEC	) (HI	GH S	PEED	SHAF	<u>T)</u>			
100	B.5	10	10	9,11	51730	7.29	41384	6.07	34487						150	
150	I	ł	10	6.36	51730	5.09	41384	4.24					1 1		660   097	
200	1		20	5.47	56097	4.38	44878	3.65	37398	3,13	32055	5 . 69.2	'	30		
				2.00	56097	3.12	44878	2.60	37398	8 2.23	3205	5 64.6	3 L		097	N
300	I .		20 20	3.90	56097	2.43	44878	1		,	3205				097	O T
400 500	1			2.65	52325	2.12	41860		3488	3   1.51	29900	0 53.2	1	2.65 52	325	т
	1	'0									3191	4 52.3		2.40 55	849	R
600	1,42			2.40	55849	1,92	44679						1		323	E
750	1			2.01	54323	1.61	43458 41860					1	1		2325	Q
1000	.85	50 20	50	1.52	52325	1.22	41000	, ,,,,								Ü
1200	,   -/	08 30	40	1.50	57523	1.20	46018		3834			i i			7523	i R
1504		57 50		1.22		.976		8.			97 3157		1		5257 5257	e E
180		72 60		1,07		.856	44206	5 .7	13 3683	.6	11 3157	r5 38.i		1.07 3	JEJI	ם
	1	į.				1	1467		57 3723	33 5	63 3191	14 38.	2	.986 5	5849	
200		25 50		i		.789			83 3723		99 3191		1 1		5849	
240	I	54 60				,			71 3488	1	03 2990	00 33.			2325	
360		83 66						i i	39 2793		90 2394	46 30.	9	.508 4	1905	i

OVERHUNG LOAD-LOW SPEED SHAFT — MODELS 8001 AND 8004 7,000 LBS. AT CENTER POINT OF SHAFT EXTENSION.

MODELS 8007 AND 8008 — OHL\* 9,800 LBS., TO\* THRUST OUT 8,300 LBS. AND TI\* THRUST IN 6,500 LBS.

MODELS 8009 AND 8010 7,000 LBS. AT CENTER POINT OF SHAFT EXTENSION. THRUST\* UP OR DOWN 6,500 LBS.

\*OHL and Thrust values shown are independent functions and cannot be applied simultaneously. Refer applications with combined OHL and Thrust to Hub City Customer Service

Denatingent

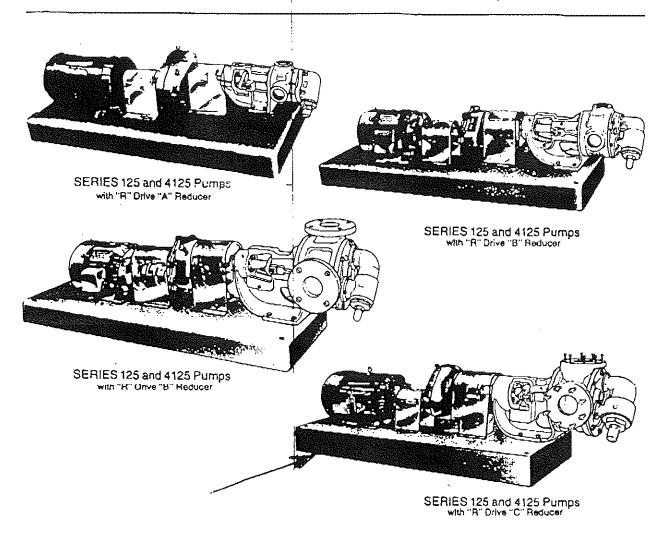
Thermal capacity can be improved on some applications with the addition of a fan on the primary unit. Consult Hub City Customer Service for specifics.



## SPAIGUE

VIKING HEAVY-DUTY PUMPS SERIES 125 AND 4125

#### VIKING HELICAL GEAR REDUCTION UNITS ("R" DRIVE)



Viking's heavy-duty pump Series 125 and 4125 are available with helical gear reducers that have been specifically developed for efficient operation with Viking heavy-duty pumps. These rugged, compact, exceptionally quiet gear reducers come in three sizes: the "small" A size, "medium" & size and "large" C size.

Beizo and "largo" Coiso.

The "A" electeduore, available with four-goor sation (2.24, 2.76, 3.43 and 4.17 to 1), is ideally suited for use with the "G," "H," "HL," "AK" and "AL" size pumps. This reducer is bracket mounted and requires couplings on both the input and output chafts. With the "A" size orduor and 1200 or 1800 RPM motors, the "G," "H," "HL," "AK" and "AL" size pumps can be used to cover a capacity range from 1.2 to 51 GPM.

The medium size "B" helical gear reducer is available with six gear ratios from 2.76 to 1 to 7.65 to 1. This size normally is used with pump sizes "AK" through "LS." Like the

"A" reducer, the "B" reducer is bracket mounted and requires couplings on both the input and the output shafts. With the "B" reducer, "AK" through "LS" pumps driven by 1200 or 1800 RPM motors can be used to cover a capacity range from 6 to 213 GPM.

The large "C" eise reducer also is available with eix gear-ratice from 2.80 to 1 to 7.95 to 1. It is normally used with the "KK" through "M" size pumps. Like the "A" and "B" reducers, the "C" reducer is bracket mounted and requires flexible couplings both for the input and output shafts. With the "C"-reducer, "KK" through "M" eise pumps, driven by 1200 or 1800 RPM motors, can cover a capacity range from 15 to 410 GPM.

Dimensions for "R" Drive Units—See Pages 141.12 and 141.13. Performance Data for "R" Drive Units—See Pages 141.17 through 141.42.

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## VIKING HEAVY-DUTY PUMPS

## **SERIES 125 AND 4125**

#### VIKING HELICAL GEAR REDUCTION UNIT ("R" DRIVE)

#### HELICAL REDUCER SPECIFICATIONS AND PUMP CAPACITY TABLE—"A" SIZE

***************************************		_		FUMP MODELS AND CAPACITY BPM D WITH												
11-1	Reducer	Ĵ⊭ai. Motor	P	G125R o	G4128R	¥125R a	r H41258	HL125A s	r HL4125A	ÁX125F 0	CAECIZSA	AL 125A D	r AL 4125A			
Major RPM	RPM Ratio MP	Pvenp RPM	50 P\$1	100 PS!	50 P\$1.	190 PS1	50 P\$1	100 PBI	56 P31	100 P81	80 831	100 781				
	2.24 to 1	5	78Q	3.7	33	8.6	6.3	13.4	13.0	36.5	36.0	51	50			
	2.76 to 1	5	540	2.8	2.5	5.3	5.1	10.9	10.5	29.5	29.0	42	41			
1800	3.43 to 1	3	520	2.2	1.8	4.2	3.9	8.6	8.2	23.8	23.3	34	3.3			
	4.17 to 1	3	420	1.7	1.3	3.3	3.0	6.6	8.4	19.2	18.7	27	26			
	2.24 to 1	3	520	2.2	1.8	4.2	3.9	8.6	8.2	23.8	23.3	34	33			
	2.78 to 1	3	420	1.7	1.3	3.3	3.0	6.8	5.4	19.2	18.7	27	26			
1200	3,43 to 1	2	350	1.2		2.6	2.3	5.4	5.0	15,3	14.8	23	22			
	4.17 to 1	2	280		1	2.0	1.7	4.2	3.8	11.0	10.5	18_	17			

#### HELICAL REDUCER SPECIFICATIONS AND PUMP CAPACITY TABLE-"B" SIZE

	· .		ſ				₽U≱	PHODE	(\$ NXO C	APACITY	б₽₩Ф У	alth Bise	.,9,, MEDA	cea			
	<b>.</b>	J. Mar.	Buss		SR or 1258		SR or 1258		5R pr 1257		8A or 125R		L01288, L04128R		SR or 1125	L84	\$A ≥r 1258
Motor NPM	Reducer . Ratio	Molar HP	Pump RPM	\$0 P81	100 PSI	50 PSI	100 P\$1	50 PSI	100 PSI	50 P\$1	100 PSI	50 P\$1	100 PBI	50 PSI	100 P81		100 P\$I
	2.75 to 1	15	640	29.5	29.0	4	41	65	54	84	83	144	143			213	508
	3.40 to 1	10	520	23.8	23 3	34	33	53	52	68	58	117	115	147	146	172	166
1800	4.19 to 1	10	420	19.2	18.7	2	26	42	41	54	53	94	83	117	116	136	134
,,,,,	5.06 to 1	10	350	15.3	14.8	28	22	35	34	44	43	77	76	96	95	115	111
	6.27 to 1	712	280	11.0	10.5	110	17	27	26	34	33	81	60	75	74	80	8.6
	7.85 ID 1	5	230	<u> </u>	1	1		\$2	21	27	26	50	49	61	60	74	70
	2.76 to 1	10	420	19.2	18.7	27	26	42	41	54	53	94	93	117	116	138	134
	3.40 to 1	10	350	15.3	14.8	20	22	35	34	44	43	77	76	96	95	115	111
	4 19 to 1	7:7	280	12.0	11.5	18	17	27	26	34	33	61	60	75	74	90	8.6
. 200	5.06 to 1	71/2	230	10.0	9.5	1 15	14	22	21	27	26	50	49	61	60	74	70
1200		5	190	8.0	7.5	1 7	11	18	17	.22	21	40	39	50	49	59	5.5
	6.27 to 1	<del>-</del>			5.5	9	1 8	14	13	17	16	31	30	36	37	47	43
	7.65 to 1	\$	155	6.0	5.5	1 7	1 8		1 1/2	<u> </u>		J	<u> </u>	<del></del>	<del></del>		

#### HELICAL REDUCER SPECIFICATIONS AND PUMP CAPACITY TABLE—"C" SIZE

		· · · · · · · · · · · · · · · · · · ·	T	T		PUE	P MODELS A	KO CAPACIT	KIN DHOS A	SIZE "C" RE	DUCER		-005-00-0
[		Ţ muaita⊭		EK125A EK4125A		LQ128R	LL12	5R 64 25R	L8125R or L\$4125R	012	58 or 258	M125 M412	BR.
MOIST RPM	Reducer Ratio	Motor Kp	Pymo RPM	200 PSI	150 PSI	200 P\$I	130 PE	200 P81	150 P\$I	50 PSI	100 PSI	50 P21	75 P8
	2.80 to 1	40	640	82	142	141	,		205			<u></u>	
•	331 to 1	40	520	6.5	115	114	145 -	143	184	307	302	<u>.</u>	
}	4.21 10 1	30	€20	52	92	91	115	113	130	241	236	410	403
		25	350	42	74	74	94	92	107	( 193	188	335	328
1800	5.08 10 1		<del></del>	<del></del>	59	58	73	71	82	145	120	257	250
	6.24 to 1	20	280	32	<del></del>			57	66	115	110	205	198
	7.95 to 1	15	230	25	6.8	47	59	<del>,                                    </del>		<u> </u>	236	410	403
	2.80 to 1	30	420	52	93	91	115	113	130	241		1	328
	3.31 to 1	25	350	42	75	74	84	92	107	193	186	335	·
	4.21 10 1	20	280	32	50	5-8	73	71	82	146	140	257	250
		1	230	25	44	47	59	57	86	115	110	205	198
1200	5.08 to 1	50	<del></del>		1 7		48	48	51	89	84	160	163
	6.24 to 1	15	190	20	34	37	1	<u> </u>	1		59	122	115
	7.95 to 1	10	155	15	29	28	36	34	33	54	<u> </u>	1 .54	<u> </u>

Recommended maximum motor horsepower based on 8-10 hour per day service (Service Factor of 1.0). For other time length of service per day, see Service Factor lable and Reducer Horsepower tables in General Catalog Section.

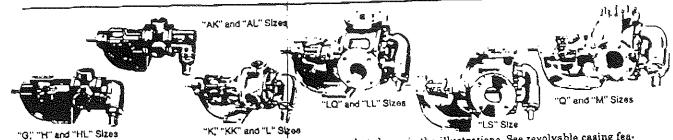
<sup>610</sup> or Technical Service Manual (TSM-610) to determine reducer capabilities.

<sup>©</sup> Capacities are based on 100 SSU liquid and 15" Mercury Vecuum.

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#### VIKING HEAVY-DUTY PUMPS **SERIES 125 AND 4125**

#### UNMOUNTED PUMPS



This series of heavy-duty pumps is available either unmounted or mounted units as shown on following pages. Available with Multi-Ring stuffing box or Buna-N mechan-Ical seal with Larbon rotating and Ni-Regior etationary faces. The integral thrust boaring is designed to handle heavy-duty pumping jobs without problems of end play and distortion. For increased versatility of installation and complete selection of ports, the pump casing is designed so it can be rotated on the bracket to any 45° or 90° angle from

that shown in the illustrations. See revolvable casing feature on Page 141.3. Pressure relief valve on head is standard for this series. To permit use of this type pump in a greater range of applications, some sizes are available with jacketed head plate. For neavy-duty pumps with jacketed bracket and head, see Catalog Section 142.

Dimensions for Unmounted Pumps-See Page 141.11. Performance Data for Unmounted Pumps - See Pages 141.17 through 141.42.

### CONSTRUCTION—SERIES 125 AND @4125 ("G" THROUGH "M" SIZES)

,011311100		7		1				Bus)	ilngr		interna:
1		<b>\</b>		į	1	Remether.	Pas	keu	Ma ch	Coal	Pellef
PTUTRE .			Bracket	Rotor	ildler	BAG HTS/6784	ldjer	Bracket	ldiar	Brackel	Asjaā
Construction	Çasing	Heed	DISCROL	110101	++		<u> </u>	D	Carbon	- Ø Bronze	Iron
Outsider	tron	Iron	HOH	20 huji-	Iran	Steel	Rrqn24	Bronze	Gracato		<del></del>
Construction		<del> </del>	ļ	912-1	W lens	Sreel	Bronze	Bronz*	Carbon	& Bronze	1ran
Fitted	itan	1 ""	Hote	d.25.	10.13.22		0.0120		Carbon		
Ø Bronze	-			<b>⊙</b> Bronze	Bronze:	Steel	Bronze	8ronze	Graphite	® Bronze	lron
Simuel	Frou	tron	[tou	00000	101012	1					

#### SPECIFICATIONS—SERIES 125 AND @4125 UNMOUNTED PUMPS

Mode!	Port	(E) Pur Pur	) inai 155	Mete Regal Pated Pam	ned ki Dpood ping	Maziraum Hyd-o Static Proceuro	Sizel Fittsd Construction Researched Above This Viencelty	© Max. Rec. Discharge Pressure Mandino 109 85U Liquid At Reted Speeds	Recom Temper (Leus	ក្រសិនក្នុ ស្រាស្តិត ខ្ពស់ យ៉ាទីយខ្ពស់	Mitta Astas Suibbjud Suibbjud Suibbjud
	0120					· Belia	8611	! raig	Pophod	ise,ট ≉ুল	Paunds
D Much, Soal	Inches	GPM						THE RESERVE TO SHARE	300	225	22
G4125	1				176		<u> </u>		300	225	- 30
₩±17¢	11/4	15		11/2	2				200	225	40
HL4125	11/2	30	1800	2	3					225	76
	7	50	1200	3	5	400				225	81
		75	1200	5	716	400	Ø25.000				105
				1-3	710	400	7	200		1	110
K4125	<del>-</del> -			<del>  _</del>		-	26,000	200	300	<u> </u>	
	2					11		200	300		155
	<u></u>			<del></del> -				200	300		175
LQ4125								200	300	225	185
LL4125	<b>3</b> ⊕3	140	520	71/2					300	225	190
1 54125	103	200	640	15	20	400				725	440
		300	520	20	30	400	7,500				600
					40	400	25,000	150	300		·
	Modal umber  U & Mech, Seai G4125  U-125  U-125  AL-125  K4125  K4125  K4125  L-125  K4125  L-125  K4125	Mindal with Side W 9 Mach, Seal Inches G4125 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Mach. Seal   Inches   CPM   C4125   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2   1/2	### Port   ### Pump   ### Pump	Port   Pump   Pump	Modes   Port   Pump   Required & Pumpler	Model	March   Port   Pump   Pump	Model   Port   Pump   Pump	March   Port   Pump   Pump	April

- () Buna-N eladomer usou neurodiscioni bool el corise 4174 manna
- TG" and "Q" sizes have steet idler.
- For mechanical seal pumps on applications with viscosities jabove 15,000 SSU, provide details for recommendation.
- Pons are suitable for use with 125# ANSI castiron or 150# ANSI steet com-panion flanges or flanged littings. All others tapped for standard pipe.
- (3) Standard seal can be wood from 20°F, to + 225°F. With special construction, temperatures from -our F, to + 650°F, can be handled with this sarias
- ① Nominal rating based on handling thin liquids.
- TAK " "AL " "KK" and "LS" sizes have Ductile Iron retor

- O For maximum recommensum utality to propoure when herefing other viscoures around when speeds, see parameter nives. Parlormetric curves also show preferred constructions, if suction presoure exceeds 50 PSIG. consult factory.
- ① Check factory before using bronze rotors at viscosities normally requiring gleet fitted construction. "G." "AK," "AL" and "LS" sizes not available in
- Bleet litted construction. G. "AK, "AL" and "LS sizes not available in bronze fitted construction.
  "AK", "AL", "LS", "Q" and "M" 4125 models furnished with carbon graphite bracket buchings and mechanical seal is mounted in stuffing box. Mechanical seal is mounted behind roter in "Q", "M", "HI", "K", "KK", "L", "LO" and "LL" pumps.
- TAK" and "AL" sizes not available in stabliffixed construction.

*-		<b>.</b> .		*		*
					•	

Greenville, SC (803)299-0135 Chesteroogs, TH (615)855-1417 Releign, NC (819)832-8634 Kreunièr, Th (615)838-7728

Wireton-Salem, №C (919)723-1683 Keste(ile, Tri (616)350-6080

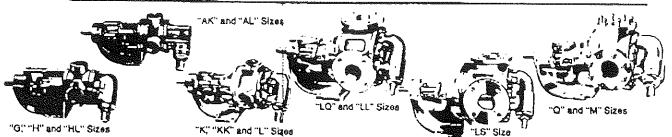
Columbia, SC (803)799-8090



#### VIKING\* HEAVY-DUTY PUMPS **SERIES 125 AND 4125**

#### UNMOUNTED PUMPS

**3004116, NC (704)887-4538** 



This series of heavy-duty pumps is available either unmounted or mounted units as shown on following pages. Available with Multi-Ring stuffing box or Buna-N mechanical seal with carbon rotating and Ni-Resist stationary faces. The integral thrust bearing is designed to hardle heavy-duty pumping jobs without problems of end play and distortion. For increased versatility of installation and complete selection of ports, the pump casing is designed so it can be rotated on the bracket to any 45° or 90° angle from

that shown in the illustrations. See revolvable casing feature on Page 141.3. Pressure relief valve on head is standard for this series. To permit use of this type pump in a greater range of applications, some sizes are available with jacketed head plate. For heavy-duty pumps with jacketed bracket and head, see Catalog Section 142.

Dimensions for Unmounted Pumps-See Page 141.11. Performance Data for Unmounted Pumps—See Pages 141.17 through 141.42.

#### CONSTRUCTION-SERIES 125 AND #4125 ("Q" THROUGH "M" BIZES)

1					,	9 a to - 5 b a 8	-	Bus	aşalıf		
Pump						Roter Shaft and	Pac	ied	Mach	. Sep!	internat Relief
Construction	Cezing	Hend	Brecket	Hotor	1∉ ef	ider Pin	ldier	Bracket	ldler	Brackel	Valva
Standard Construction	kon	Iron	Iron	<b>⊙</b> Iron	l <b>e</b> on.	Ste⇔l	Bronze	Bronze	Carbon Graphite	⊗ Bronze	lron
®Steel Fitted	lm	Iron	Iron	Steel	(D) ron	Steel	Brónze	Bronze	Carbon Graphite	<b>⊕</b> Bronze	Iron
®Bronze Fined	lron	Iron	[ron	® Bronze	Втопае	Steel	Bronze	Bronze	Carbon Graphite	<b>®</b> Вголие	nosi

#### SPECIFICATIONS—SERIES 125 AND @4125 UNMOUNTED PUMPS

	Model Yumber	Port Siza	Pu	D dest mp ing	Requi Reled Pur	or HP tred At Speed sping U Liquid	ļi	essace grassic Agus- squassus-	Steel Fitted Construction Recognimended Above This Viccestry	(B) Max. Acc. Discharge Pressure Handling 100 380 Liquid At Rated Speeds	Recon Tempe Cat	izimum imended ratura for ologed sp. *F.	Approximate Shipping Weight With Valve
Packed	O Mech. Lea!	inches	GPM	RPM	50 P\$I	100 981		PSIQ	680	i PSIG	Packed	Mach. Sesi	Pounds
G125	G4125	1	8	1800	¥,	11/2	Τ	400	7,500	. 200	300	225	22
H125	H4125	11/2	15	1800	11/4	2	Т	400	25,000	200	300	225	38
HL125	HL4125	11/h	30	1800	5	3		400	7,500	200	300	225	40
AK125	AK4125	2	50	1200	3	5	Т	400 .	\$25,000	150	300	225	78
AL125	AL4125	2	-75	1200	5	71/2		400	\$25,000	150	300	225	81
K125	K4125	2	60	640	3	71/2	Т	400		200	300	226	105
KK125	KK4125	2	80,	640	5	71/2	T	400	25,000	200	300	225	110
L125	L4125	2	135	640	71/2	15		400	25,000	. 200	300	225	155
LQ125	LQ4125	<b>D21</b> /2	135	840	71/2	15	$\top$	400	25,000	200	300	225	175
LL125	LL4125	@3	140	520	712	15	十	400	2.500	500	300	225	185
LS125	LS4125	<b>©3</b>	200	640	15	20	1	400	75,000	150	300	225	190
Q125	Q4125	<b>@</b> 4	300	520	20	30	1	400	7,500	150	300	225	440
M125	M4125	<b>@</b> 4	420	420	20	40	1	400	25,000	150	300	225	600

- Buna-N elastomer used in mechanical seal of Series 4125 pumps.
- @ "G" and "Q" sizes have steel lider.
- ② For mechanical seal pumps on applications with viscosities above 15,000 SSU, provide details for recommendation.
- ⊕ Porte are suitable for use with 125# ANSI cast kon or 150# ANSI sized companion lianges of flanged littings. All others tapped for standard pape.
- Standard seat can be used from 20°F, to 225°F. With special construc-tion, temperatures from 80°F, to + 650°F, can be handled with his series
- D Nominal rating based on handling thin liquids.
- O "AK," AL," "KK" and "LS" sizes have Ductile from rotor

- D For maximum recommended discharge pressures when handling other viscosities and/or other speeds, see performance curves. Performance curves also show preferred constructions. If suction pressure exceeds 50 PSIG. consult factory.
- Thack factory before using promite rotors at viacosities normally requiring steel fitted construction. "G." "AK," "AL" and "LS" sizes not available in bronza litted construction.
- "AK", "AL", "US", "Q" and "M" 4125 models furnished with carbon graphite bracket bushings and mechanical seal is mounted in stuffing box. Mechanical seal is mounted behind rotor in "G", "H", "HL", "K" KK", "L", "LQ" and "LL" pumpe.
- Tak" and "AL" sizes not available in steel fitted construction.

4.		٠.		t.		



## Tank Protection Division

- □ Sizes 2" through 12"
- ☐ Pressure settings ½oz/in² to 15 PSIG
- $\Box$  Vacuum settings  $\frac{1}{2}$  oz/in<sup>2</sup> to 12 PSIG
- Available in aluminum (type 356), carbon steel, stainless steel and other materials.
- Modular construction

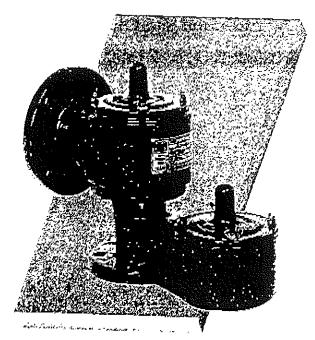
#### PRESSURE / VACUUM RELIEF VALVE WITH PIPE-AWAY FEATURE

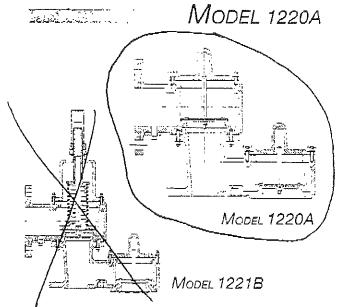
Model 1220A is used for pressure and vacuum relief where vapors must be piped away. Special pallets in the Model 1220A housing virtually eliminate the intake of air and the escape of vapors except during normal tank breathing, thus reducing the loss of product. These special pallets are engineered to allow only the intake or outlet relief necessary to maintain the proper working pressure, thereby protecting the tank from possible damage. Escaping vapors are piped away through a flanged outlet connection. This helps to provide increased fire protection and safety.

#### SPECIAL FEATURES

Model 1220A offers Groth's special "cushioned air" scating. Superior performing Teflon's seating diaphragms are standard to minimize sticking caused by resinous vapors and atmospheric moisture. The Model 1220A has a self draining housing body and drip rings to protect seating surfaces from condensate and freezing. This design also avoids pressure or vacuum buildup due to binding or clogging of the valve. Buna-N, Viton's and other seating diaphragms can be provided when required. Model 1221B may be spring loaded when required for use on blanketed tanks or other type installation requiring higher settings. To insure the proper alignment of seating surfaces there is peripheral guiding and a center stabilizing stem.

# Pressure/Vacuum Relief Valve with Pipe-Away Feature Model 1220A





## GROTH, THE CAPABILITY COMPANY

As with all Groth products, every Model 1220A is factory inspected and tested to meet your critical requirements and special needs. Inventory is maintained to insure rapid delivery.



THIS CHART SHOWS CAPPOLITIES FOR PRESSURE/VACUUM VENT WITH FLAME ARRESTER

### PRESSURE RELIEF CAPACITY

## MODEL 1220A/7618

1	ressure P <sub>s</sub> )	Air Fl	Air Flow Capacity at 100% Over-pressure (Double Set Pressure) 1000 Standard Cubic Feet per Hour at 60° F									
In WC	Oz/Sq In	2"	3"	4"	6"	8"	10"	12"				
0.87	0.50	2.92	5.68	10.3	20.7	32.3	51.5	59.1				
<del>  →</del> 1.00	0.58	(3.19)	6.34	11.5	23.3	36.2	57.6	67.8				
1.73	1.00	4.45	9.23	16.8	34.4	53.0	84.4	105				
2.00	1.16	4.84	10.1	18.5	37.8	58.2	92.6	116				
2.60	1.50	5.64	11.9	21.7	44.6	68.5	109	138				
3.00	1.73	6.12	13.0	23.7	48.8	74.8	119	151				
3.46	2.00	6.65	14.1	25.9	53.2	81.6	130	165				
4.00	2.31	7.21	15.4	28.2	58.0	88.9	141	180				
6.00	3.47	9.07	1 <b>9</b> .5	35.7	73.6	113	179	230				
8.00	4.62	10.7	23.0	42.1	86.8	133	211	272				
10.0	5.78	12.1	26.1	47.7	98.6	151	240	309				
12.0	6.93	13.3	28.9	52. <del>9</del>	109	167	266	343				
15.0	8.66	15.1	32.7	60.0	124	189	301	389				
20.0	11.6	17.7	38.4	70.4	146	222	354	457				
25.0	14.4	20.0	43.5	79.7	165	252	400	518				
30.0	17.3	22.2	48.1	88.2	182	278	443	574				

Flow capacity is certified by Groth Corporation, based on actual tests conducted in compliance with API Std. 2000. Flow measurement accuracy has been verified by an independent testing laboratory.

Flow copacity values listed above are based on full open valves at 100% over-pressure.

Consult Factory for flow copacity with fiberglass valve.

Read the flow capacity at 100% over-pressure directly from the table above. Use linear interpolation if the ser pressure is not listed. (Reft. Page TPD1)

If the allowable over-pressure is less than 100%, modify the flow capacity using the appropriate "C" factor from the table. If allowable over-pressure is more than 100%, consult page TPD1 or your Groth Representative.

Calculate the percentage over-pressure by the following formula. More that all pressures are gage prossure expressed in the same units of measure.

 $P_F = Flowing pressure$ 

P; = Sat pressure

 $\Re OP = [(P_1 - P_2)/P_2] \times IOO$ 

Calculate flow capacity of less than 100% over-pressure according to the following ехотр.е.

#### Example—flow Capacity Calculation

- 6" Model 12204/7618
- 4 In WC set pressure [P,]
- 7 in WC flowing pressure [P<sub>f</sub>]
- 1. Read flow copecity at set pressure from table
- 2. Colculate over-pressure
- 3. Read "C" fector from toble
- 4. Calculate flaw capacity

Example—To find "C" factor from table:

Read "C" factor for 75% Over-pressure at intersection of row 70 and column 5 "C" factor of 75% OP = 0.87

"C" Factor Table												
%0P	Ô	1	2	3	4	5	6	7	8	9		
10												
20		Consult										
30					Factory	ı						
40	:											
50	0.72	0.73	0.73	0.74	0.75	0.75	0.76	0.77	0.77	0.7		
60	0.78	0.79	0.80	0.80	0.81	0.81	0.82	0.82	0.83	0.8		
70	0.84	0.85	0.85	0.86	0.86	0.87	88.0	0.88	0.89	0.8		
80	0.90	0.90	0.91	0.91	0.91	0.92	0.93	0.93	0.94	0.9		
90	0.95	0.95	0.96	0.96	0.97	0.97	0.98	0.99	0.99	1.0		

Flow = 58,000 SCFH

 $\% \text{ OP} = [(7-4)/4] \times 100 = 75\%$ 

 $10^{\circ} = 0.87$ 

 $Flow = 0.87 \times 58,000 = 50,460 SCFH$ 



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VACUUM CAPACUTY FOR VENT & FLAME ARRESTER COMBINATION

### VACUUM RELIEF CAPACITY

## MODEL 1220A/7618

Į.	acuum P <sub>s</sub> )	Air Flow Capacity at 100% Over-vacuum (Double Set Vacuum) 1000 Standard Cubic Feet per Hour at 60° F										
In WC	Oz/Sq In	2"	3"	4"	6"	8″	10"	12"				
0.87	0.50	2.55	5.19	8.80	17.9	28.6	44.3	53.6				
→ 1.00	0.58	(2.77)	5.73	9.70	19.8	31.6	48.9	60.4				
1.73	1.00	3.78	8.15	13.6	28.3	45.1	69.4	89.8				
2.00	1.16	4.10	8.90	14.9	31.0	49.3	75.8	99.0				
2.60	1.50	4.74	10.4	17.4	36.2	57.7	88.6	117				
3.00	1.73	5.14	11.3	18.9	39.5	62.9	96.0	128				
3.46	2.00	5.56	12.3	20.5	42.9	68.4	105	139				
4.00	2.31	6.03	13.4	22.3	46.7	74.4	114	152				
6.00	3.47	7.54 <sup>1</sup>	16.9	28.1	58.9	93.8	144	193				
8.00	4.62	8.84	19.9	33.0	69.4	110	169	227				
10.0	5.78	10.0	22.5	37.4	78.6	125	192	258				
12.0	6.93	11.1	24.9	41.5	87.1	139	212	286				
15.0	8.66	12.5	28.2	46.9	98.6	157	240	324				
20.0	11.6	14.7	33.1	55.1	116	184	282	381				
25.0	14.4	16.6	37.5	62.3	131	209	319	432				
30.0	17.3	18.3	41.5	68.9	145	231	353	478				

flow capacity is certified by Groth Corporation, based on actual tests conducted in compliance with API Std. 2000. Flow measurement accuracy has been verified by an independent testing laboratory.

Flow copacity values listed above are based on full open valves at 100% over-vacuum.

Consult Factory for flow capacity with fiberglass valve.

Read the flow copacity at 100% over-vacuum directly from the roble above. Use linear interpolation if the set vacuum is not listed. (Ref. Page IPD1)

If the allowable overvacuum is less than 100%, modify the flow coocciry using the appropriate "C" factor from the table. If allowable overvacuum is more than 100%, consult page TPD1 or your Groth Representative.

Calculate the percentage avervacuum by the following formula. Note that all pressures are gage pressure expressed in the same units of measure.

 $\begin{array}{l} P_f = \mbox{FlowIng pressure} \\ P_s = \mbox{Set pressure} \\ \% \mbox{ OV } = [(P_f - P_s)/P_{s^2} \times \mbox{ i 00} \end{array}$ 

Calculate flow capacity at less than 100% over-vacuum according to the following

#### Example—Flow Capacity Calculation

6" Model 1220A/7618

4 In WC set vacuum (P<sub>c</sub>)

7 In WC flowing vocuum (P.)

- 1. Read flow copacity at set vacuum from rable
- 2. Calculate over-vacuum
- 3. Read "C" factor from table
- 4. Colculate flow copocity

Example—To find "C" factor from table:
Read "C" factor for 75% Overvacuum at intersection of row 70 and column 5 "C" factor or 75% OV = 0.87

	"C" Factor Table												
%0V	0	1	2	3	4	5	6	7	8	9			
10	İ												
20	   	Consult											
30		Factory											
40	: :	·											
50	0.72	0.73	0.73	0.74	0.75	0.75	0.76	0.77	0.77	0.78			
60	0.78	0.79	0.80	0.80	0.81	0.81	0.82	0.82	0.83	0.84			
70	0.84	0,B5	0.85	0.86	0.86	0.87	0.88	0.88	0.89	0.89			
80	0.90	0.90	0.91	0.91	0.91	0.92	0.93	0.93	0.94	0.94			
90	0.95	0.95	0.96	0.96	0.97	0.97	0.98	0.99	0.99	1.00			

Flow = 46,700 SCFH

 $\% \text{ OV} = \{(7 - 4)/4\} \times 100 = 75\%$ 

"C" = 0.87

 $Flow = 0.87 \times 46,700 = 40,629$  SCFH

	*.		*		V.	
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4						



## FLAME ARRESTERS MODELS 7618/7628

	Sizes	2"	through	60"
--	-------	----	---------	-----

- Available in, carbon steel, stainless steel aluminum (type 356) and other materials
- Wafer design for quick and easy maintenance
  - Unique recessed seating for superior protection
  - Factory Mutual approval for most sizes and materials
  - Proven spiral wound, crimped ribbon, flame element

#### FLAME ARRESTER

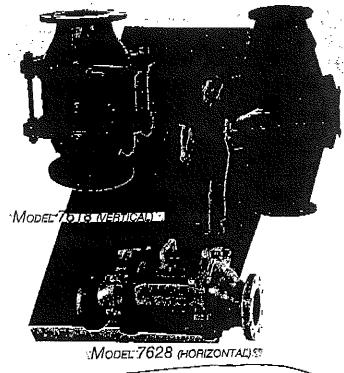
Both models are designed to inhibit flame propagation in gas piping systems and to protect low pressure tanks containing flammable liquids. Arresters protect low flash point liquids from externally caused sources of heat and ignition. This provides increased fire protection and safety.

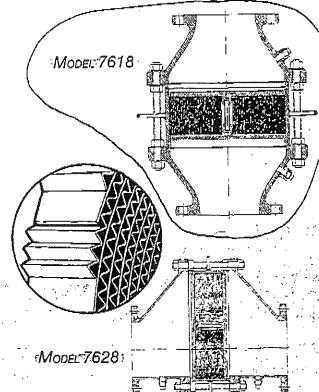
#### SPECIAL FEATURES

Both models are built of corrosion resistant materials throughout. Wafer design construction affords easy accessibility to the flame bank. Additionally, jack screws aid in the removal from the shell assembly. All Groth flame arrester flame banks utilize spiral wound, crimped ribbon constructed flame elements. These proven, Factory Mutual approved elements have been reported, by NTIS of the Dept. of Commerce, to provide the best flame quenching performance for the least pressure drop. Groth's special recessed flame bank scaring construction uniquely provides an extra measure of protection against leakage and possible flame propagation.

## GROTH, THE CAPABILITY COMPANY

As with all Groth products, every Flame Arrester is factory inspected and tested to meet all critical requirements and special needs. Inventory is maintained to insure rapid delivery.





Note: All Groth Flame Arresters are Bi-directional. Factory Mutual regulates that Flame arresters be installed with 10 pipe diameters of the source of ignition.

			:
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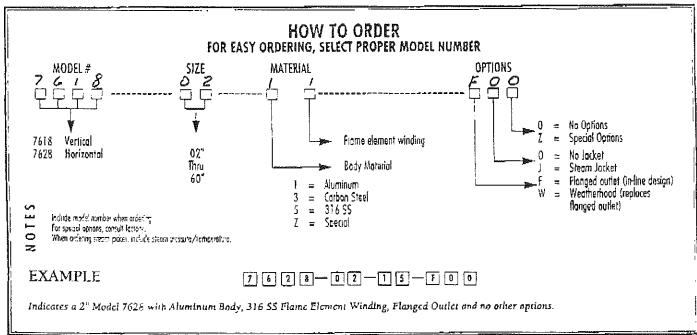
LAVA

ರೈಕ್ಷಪ್ರಾಗ್ರೆಕ್ಕೀಕಿಂಗತ ತಟ್ಟಾಂದ 10 ohongo ಅಕ್ಷಿಗಿರುಗ ನಿರ್ವಾದ	Camified dimensions (svalleble upon requosit,
-------------------------------------------------------------	-----------------------------------------------

(-110) 34(23 Yu 10) 27/01/10.2. 30/00002033 4 I

(51 mm) 3" (76 mm) 4" (102 mm)	8;" (721) 9;" (241) 11;" (292)	14" (256) 16" (406) 181" (464)	134" (549) 157" (400° 18"	9 ‡ " (741) 11" (279) 12 ‡ "	50 PSIG (\$45 kPe) 50 PSIG (\$45 4Pe) 50 PSIG	100 PSIG (693 PPc) 100 PSIG (690 kPc) 100 PSIG	150 PSIG (1025 kPc) 140 PSIG (966 kPo) 140 PSIG	350 PSIG (2415 kPpl 325 PSIG (2242 kPp) 325 PSIG	18 (8kg) 25 (11 kg) 40
3" (76 mm) 4" (102 mm) 6"	9½" (241) 11½"	16" (406) 184"	(400°	(279) 12 <del>†</del> "	(345 4Pa) 50 PSIG	(690 k²a)	(966 kPa)	(1242 kPa)	(11 kg)
(102 mm) 1	i i			!		100 PSIG	140 PSIG	325 PSIG	40
i I				(316)	(345 kPa)	(693 FPa)	(966 kfol	(2242 kPa)	( ' ŝ kç )
,	16 ; "	21"   (531)	21" (535)	16 ÷ " (419)	50 PSIG (2/5 kPc)	100 PSIG	140 PSIG	325 PSIG (2242 kPa)	70 (22 kg)
8" (203 mm)	21"	25" (655)	25" (653)	20 ÷ " (521)	50 PSIG (545 +2a)	100 PSIG (690 k74)	90 PSIG (421 kPs)	200 PSIG (1380 kPa)	135 (61 kg)
10" :	24 ? "	30" (762)	30″ (767)	24 ‡" (627)	50 PSIG (\$45 kPe)	100 PSIG (\$70 27s)	75 PSIG (517 kPo)	150 PSIG (1020 kPo)	235 (127 kg)
12" (203 mm)	28 ÷"	32 ½" :825)	32 : " (376)	28 ½ " (724)	50 PSIG (\$45 k20)	100 PSIG (695 We)	75 <b>PS(G</b> (517 kPo)	150 PSIG (1035 k2a)	345 (156 kg)

Larger sizes available on special application. 150# A.N.S.I. drilling compatibility, F.F. an aluminum and R.F. on carbon steel and stainless stool alloys.





# GROTH IS COMMITTED TO THE TOTAL QUALITY IMPROVEMENT PROCESS

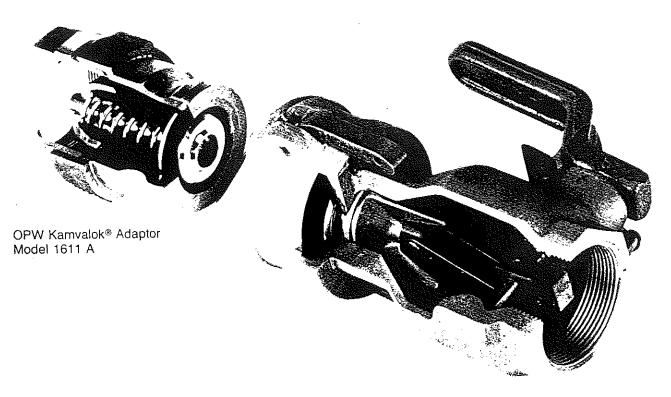
1202 Hahlo • P.O. Box 15293 Houston, Texas 77220-5293 713/675-6151 FAX 713/675-6739 Groth Products Group 1-800-552-2960 (Except Tex. & La.)



Form 101/95

SPATCO

# Opw The Dry-Disconnect Experts Introduce the D-2000 Dry-Disconnect Coupling.



OPW D-2000 Coupler Model 2261 D

If you want to avoid spillage, you need the OPW D-2000 Dry-Disconnect Cam and Groove Quick Coupling. The D-2000 helps prevent spillage from disconnect. Your product stays in the line – and off the floor.

- Easy-to-Clean Design
- Built-in Valve
- Low Cost Design
- Heavy Duty Construction

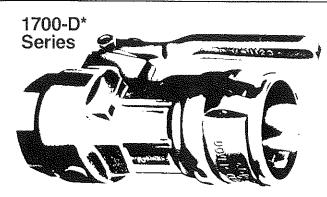
- Easy-to-Use Cam and Groove Design
- Compatible with Kamvalok Adapters
- Simple Design for Reliable Operation

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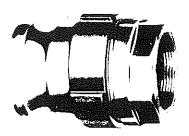
SPAICO

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# Styles



1600-A\* Series

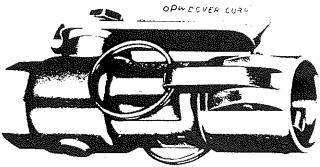


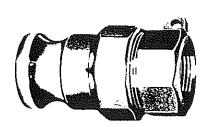
The Kamvalok® coupler and adaptor are designed with female threads, and can be fitted to either a male pipe end or to a hose fitting.

SIZES: 11/2", 2", 3"

1762-DP

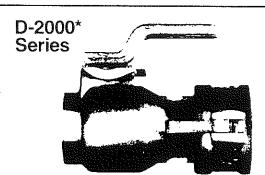
1662-A





These special Kamvalok couplers and adaptors are used primarily for low flow applications.

SIZE: 3/4"



The D-2000 coupler has been designed for applications requiring automatic closure in one direction, from adaptor side only.

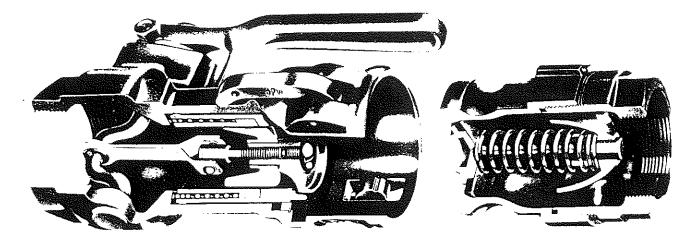
SIZES: 11/2", 2"

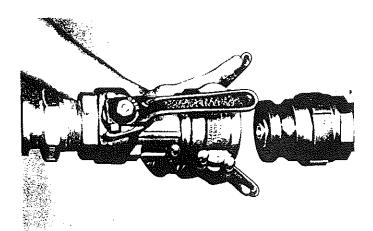
.Note: For correct product number consult availability chart specifying metal and/or seal construction.



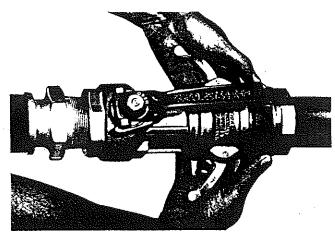
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### Operation

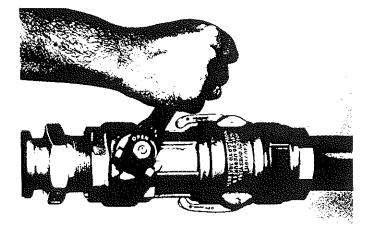




1. Couple in any position



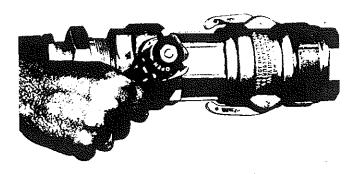
2. Cam arms lock coupler and adaptor together



3. Lever opens valve



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4. Full flow starts



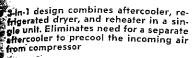
FLUID HANDLING GROUP CORPORATION / OPW DIVISION

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**PNEUMATICS** 

# REFRIGERATED COMPRESSED AIR DRYERS

# THREE-IN-ONE COMPRESSED AIR DRYERS



Handles inlet air temperature up to

Produces 35°F pressure dewpoint. Removes 96% of harmful moisture from compressed air. Helps protect air system components, spray guns, air tools, sandblasters and other pneumatic equipment

Single unit reduces installation, operating and maintenance cost

Operates in hot environments (up to 100°F maximum ambient temperature)

 All copper spiral fin tube-in-tube heat exchanger provides maximum efficiency for heat transfer and water separation

Heat exchanger warranted for 5 years

Includes monitoring instrumentation, separator, and drain trap

Standard 6 ft cord plugs into any 115V wall outlet (115V models only)

Refrigeration systems utilize environ-mentally safe R-22 refrigerant



									- renige	er anı	
s Max. Air	CFM Capacity @ 35°F Pressure Dew Point	НР	Volts, 60 Hz	Inlet/ Outlet (F)NPT	Di	mensi W	ons D	Stack No.			Shpg
- 6 10	22 37	1/3	115	1"	21"	26"	16"	5Z656	List \$1250.00	Each	Wt.
15 25	56 91	1/2 3/4 1	115 115 230	1 1 1	26 26 311s	30 30 34¼	20 20	52657 52658	1575.00 2135.00	\$1157.00 1457.00 1975.00	110.0 140.0 170.0
					31.8	3474	271/8	5Z659	3050.00	2822.00	235.0

#### ir filter to protect amb

5Z761 & 5Z762

equ red, Lun certified

areen finish

hose between air compressor o prolong equipment life. Sep-ove condensed water and oil. 1858 for separators and drains

ĸ	List	Each	. <u></u>
7 8 9 0 1	\$315.00 345.00 450.00 607.00 780.00 1040.00	\$257.75 282.00 375.00 498.00 640.00 849.00	1.6
			•

and contaminants from

ilt with corrosion resistant coppe ial baffles

movable for servicing

l aftercoolers so water flow ssed air. 250 PSI maximum water pressure. 500°F maximum ting feet at both ends. Green

List	Each	
\$203.00 229.50 448.00	\$170.75 192.00 367.25	

#### REFRIGERATED COMPRESSED AIR DRYERS

Hankison refrigerated dryers eliminate harmful moisture and provide high quality. clean, dry air.

- Consistent outlet dew points assure dry air downstream
- Built-in oil and dirt removal filter eliminates contaminants
- Large precooler/reheaters allow use of smallest refrigeration systems possible, minimizing energy requirements
- Smooth surface heat exchangers permit , low pressure drop through dryer
- Heat exchangers are fully encapsulated In non-degrading insulation to preserve cooling effect
- Efficient, direct expansion type heat exchangers respond quickly to changes in
- Non-fouling, smooth surface, copper heat exchangers maintain high heat transfer efficiency for life of dryer, no prefilter required
- Accurate control of refrigeration temperature eliminates need for manual administration temperature. justments as load or ambient tempera-

- Positive condensate discharge with compressed air powered automatic drain
- Two-stage separator maintains high efficiency separation across wide range of flows
- Refrigeration system service life maximized by continuous, non-cycling opera-
- Refrigeration systems utilize environ-mentally safe R-134A or R-22 refriger-

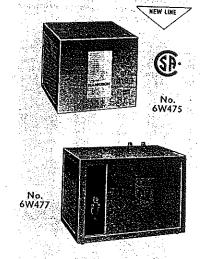
Nos. 6W474, 6W475, and 6W476 feature in Nos. 6W4/4, 0W4/5, and 6W4/6 reasure integral oil/dirt filter, power-on and high temperature warning lights, and six foot power cord with plug. Full cabinet includes removable end screens and wall mounting bracket.

Nos. 6W477 thru 6W482 have all features of No. 6W474. Also include on/off switch, refrigerant suction pressure gauge, and mounting feet instead of brackets.

Nos. 6W483 and 6W484 feature integral nos. 04403 and 04404 rearure integral oil dirt filter, and power-on, compressoron, and high temperature warning lights. Full cabinet includes removable end screens and mounting feet. Also includes

	Cilaii						re	frige	ant suc	tion n	ressure	Aiso inc gauge.	ludes
Mar. Air Cempr. HP	Dew 38°F	Cap. ssure Pts. 50°F	Come	Volts/ Phase 60 Hz	Inlet and Outlet	В	Overa imensi W	II .	Mfr's. Model	Stock	List		Shpg.
3 5 18 15 20 25 30 40 58	5 10 15 25 35 50 75 100 125 150 200	7 13 20 33 46 65 98 130 163 195 260	1/10 1/6 1/5 1/5 1/5 1/4 1/3 1/2 3/4 1	115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 460-3	3/8" OD 3/8 OD 3/8 OD 3/4" 1" 1" 1½" 1½" 2"	14" 14 14 21 25 25 25 25 36% 36%	161/s 161/s 161/s 26 26 34 34 34 34 361/s 361/s	15" 15 15 16 16 22 22 22 22 22 40 1/8 40 1/8	PR5 PR10 PR15 PR25 PR35 PR50 PR75 PR100 PR125 PR150	6W474 6W475 6W476 6W477 6W479 6W480 6W480 6W481 6W483 6W483	\$507.00 577.00 712.00 1010.00 1265.00 1690.00 2100.00 2275.00 2625.00 3250.00	\$459.50 521.50 644.50 898.00 1195.00 1620.00 2010.00 2170.00 2485.00 3095.00 3630.00	50.0 57.0 65.0 117.0 119.0 203.0 219.0 236.0 245.0 440.0





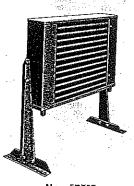
Dryer capacities at 38° and 50°F pressure Dryer capacities at 38° and 50°F pressure dew point temperatures have been established with compressed air entering dryer at 100 psig and 100°F saturated with dryer operating in 100°F ambient temperature. Operating range: 35° to 110°F ambient. Maximum working pressure: 175 psig. Maximum inlet compressed air temperature. Maximum inlet compressed air tempera-ture: 120°F. If inlet temperatures exceed 120°F, precool air with air or water cooled aftercooler.



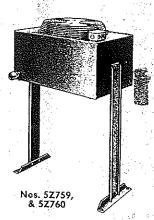
#### AFTERCOOLERS

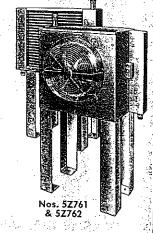
#### AIR-COOLED AFTERCOOLERS

## *SPEEDAIRE*



Nos. 5Z757-5Z760 may be mounted for either vertical or horizontal discharge





Nos. 52757, & 5Z758

Remove harmful water, oil, and contaminants from compressed air systems

- Precool hot air from compressor to temperatures required for use with compressed air dryers
- High efficiency copper tube/aluminum fin heat exchangers provide close approach temperatures with minimal power consumption
- Heavy-duty construction for long, trouble-free life
- Single point electrical junction box for ease of installation
- Includes brackets/legs for floor or suspended mounting
- Nos. 5Z759-5Z762 include ambient air filter to protect con from airborne contaminants
- Guards conform to OSHA requirements
- Fan motors are UL recognized, CSA certified
- Steel cabinets have metallic green finish

NOTE: Use of flexible metal hose between air compressor and aftercooler is recommended to prolong equipment life. Separe tor and drain required to remove condensed water and oil. 54

			o. Jospen.	idea mooning	pag	ge 2007 f	for hose a	nd page 1858	for senara	tore and deal	ine i
Maximum Comp. HP	Max. CFM @ 100 PSI*	Fan HP	Volts, 60 Hz	Inlet/Outlet (F)NPT		Dimension: W		Stock No.	List	Each	Ships
10 15 25 35 50	20 35 50 100 150 240	1/12 1/12 1/12 1/12 1/12 1/4 1/4(2)	115 115 115 115 115 115	1/2" 1/2 1 11/2 11/2 11/2 2	21 %" 21 % 42 ¼ 42 ¼ 46 ½ 49 ½	203/6" 203/8 261/8 261/8 431/2 475/8	95/8" 95/9 151/2 151/2 173/4 173/4	52757 52758 52759 52760 52761 52762	\$315.00 345.00 450.00 607.00 780.00	\$257.75 282.00 375.00 498.00 640.00	241 391 651 681 1501 2251

<sup>(\*)</sup> Ratings based on 15°F approach with 250°F inlet temperature.

#### WATER-COOLED AFTERCOOLERS



- Remove damaging water, oil, and contaminants from con pressed air systems
- Highly efficient cooler is built with corrosion resistant copf tubes, brass shell and internal baffles
- Cast iron end bonnets are removable for servicing

For best performance, install aftercoolers so water flows opposite direction to compressed air. 250 PSI maximum pressure. 250 PSI maximum water pressure. 500°F maximum operating temperature. Mounting feet at both ends. Green tallic finish. Speedaire brand.

Max. Cooling NPT  Maximum CFM @ Area Inlet & Outlet  p. HP 100 PS1 Surface Water Air	Dimensions Stock
	W H No. List Fach
0 40 3.5 sq. ft. ½" 1" 23½  5 110 5.0 ½ 1½ 1½ 365%  1 2½ 50½  aling compressed air to 15°F above inlet water temperature	3½" 3½" 5Z625 \$203.00 \$170.75

REFRIGERA

(Ein-I design combines a figerated dryer, and rehicle in the color of the from compressor changes in the color of the from compressor changes inlet air temperature.

Produces: 35°F pressure d moves: 96% of harmful m compressed air. Helps pr tin components, spray gu

(Single unit reduces install ling and maintenance cost

Dew Point HP	8
75n. 37 1.2 100 56 34 100 91 1	

. Consistent outlet dew points

downstream

sulfain oil and dirt removal

reprecooler/reheaters al plumizing energy requirem wooth surface heat exchang

u pressure drop through di Ottexchangers are fully end

then degrading insulation t uclint/direct expansion typ

Hedra respond quickly to c coace session of surface coace session of surface coace session of surface exchangers maintain in sign efficiency for life of the required Tequired

vete control of refrigeration and the eliminates need for mensional or ambient control of the co

10 13 16 115-1 38 15: 20 16 115-1 38 15: 30 15 115-1 38 15: 15-1 34 15: 15-1 34 15: 15-1 34 15: 15-1 15-1 34 15: 15-1 15-1 15-1 15: 15-1 15-1 14 15: 15-1 15-1 14 15: 15-1 14 15: 15-1 15-1 14 15: 15-1 1	FM Cap. Pressure lew Pts. LE 50°F	Refrig. Comp. HP	Volts/ Phase 60 Hz	in a: Ou
	20 33 46 65 98 130	1/6 1/5 1/5 1/5 1/4 1/3 1/2 3/4	115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1 115-1	3/8 3/4 3/4 1 1 1/2 1/2



#### AIR COMPRESSORS

# 5 TO 25 HP TWO-STAGE AIR COMPRESS

#### CHAMPION DESIGN

- For auto repair, body shops, air tool operation, and automated machinery
- All models comply with State of California Code 462 (L) (2)
- · Green finish

#### SPLASH LUBRICATED PUMPS

- Multifinned aluminum cylinder with cast iron liner combines inner strength of high density cast iron with cooling efficiency of an aluminum exterior
- 15 and 25 HP models have dual control for stop/start or continuous run operation, cast iron cylinders and heads, and an oil monitor which prevents unit from starting if proper oil level is not maintained
- Rugged, ductile iron crankshaft is counterbalanced with large diameter throws for low bearing loads
- Maximum cooling with precision balanced, fan-bladed flywheel
- Swedish steel, single-unit, plate-type valves are easy-to-service; cylinder does not need to be removed
- High density, die-cast aluminum alloy connecting rods minimize reciprocating weight
- Gasket-free integral cylinder head
- Aluminum alloy first stage piston is weight matched to second stage piston ensuring reciprocating balance
- Positive acting, governor-type, centrifugal unloader assures unloaded starts
- Unit shipped with oil in crankcase

#### MOTOR FEATURES

Dual voltage NEMA motors

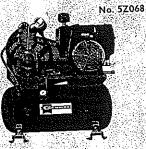
#### ENGINE FEATURES

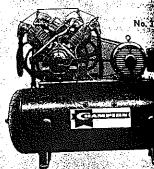
- 10 HP Kohler Magnum engine with electronic ignition
- Large capacity dual element air

#### TANK MOUNT FEATURES

 ASME tank and safety valve. Includes bucket high drain valve, 300 PSI pressure gauge, and tank shutoff valve







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	Stock No.	RPM		ump Bore	Stroke	Oil Cap.	(M)NPT Outlet	Dim
HP	5Z064 5Z065 5Z066	710	2	45/8" 45/8 21/2 21/2	3	2 qt	3/4"	32" - 37 60 kg 32 - 1 60
	5Z067	765	4	45/8	3	4	3/4	72 2
10	5Z069		$\frac{1}{2}$	21/2	3	2	3/4	41
10	5Z068	710				4	11/4	76
15	3Z412	770_	2_	61/4	41/2	<u></u>		76 .
25	3Z413	770	4	61/4	4	61/3	11/4	1 24
6003	ELECTI	RIC MO	DELS				in in the second or	netic Steri

15.7			. 3			200						Ţ	Wi	th Magnetic	2 CHILL
				Tank	Displ	CFM @	Champion	Stock No.	List	Each	Shpg. Wt.	Volts, 60 Hz	N a	List	1
не е	hase	Voltage, L	Gallons	Турв		175 PSI		E7064		\$1704.00	540.0	230	77446	\$3064.15	18
<u>s</u>	1	230	80	Vertical	20.7			5Z065			540.0			3064.1	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
5	1	230	80	Horizontal	20.7	16.5	11100		2010111			230	72448	2908.35 2906.35	
				Vertical	20.7	16.5	VR5-8	5Z066	2722.00	1602.00	540.0		7Z449		
5	3	230/460	60	V CI LICEI					2722.00	1602.00	540.0	230			
	3	230/460	80	Horizontal	20.7	16.5	HR5-8	52067				020		5115.0	5 30
		1,00,100			-		HR10-12	57069	4957.00	2882.00	890.0	460		5040.2	3 34
10	3	230/460	120	Horizontal	44.t	34.4						000		4 7142.2	2 4
_				Horizontal	61.5	5 53.7	HRA15-12	37412	6415.00	4065.00	1144.	460			<u></u>
15	3	230/460	120	Horizontal			1					1 000		6 9584.6 7 9295.6	ο 5:
		230/460	120	Horizontal	109.4					5361.00					93
25	3	230/400	120		<u> </u>		HODEL	WOHIE	P MAG	NUM EN	GINE)	)			
٠.		T	1.5	22-11-12				(KOLITE	2004.00	1917.0	0 400	0 -	_		
	<u> </u>		20	Horizontal	20.	7 16.5	HGR5-3	52068	3204.00	, 1311.0					

10 — 30 Horizontal 20.7 16.5 HGR5-3 (\*) Magnetic starters are not mounted and wired; provided separately.

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#### SECTION 13220

#### ABOVEGROUND STORAGE TANK

#### PART 1 GENERAL

#### 1.01 SECTION INCLUDES

- A. Furnish and install four 12,000-gallon carbon steel aboveground storage tanks.
- B. Furnish and install new tank accessories and controls as shown on plan sheets or specified herein.

#### 1.02 REFERENCES

- A. NFPA 30--Flammable and Combustible Liquids Code.
- B. Underwriters Laboratory--Standard for Safety 1316.
- C. File MH 9061 for storage of flammable liquids.

#### 1.03 SUBMITTALS

- A. Submit shop drawings and product data.
- B. Indicate for each tank, location of all fittings, accessories, critical dimenstions, anchoring devices, attachment, piping, and accessories.
- C. Submit manufacturer's installation and testing instructions.

#### 1.04 DELIVERY, STORAGE, AND HANDLING

- A. Deliver products to site.
- B. Store and protect products.
- C. Handle and store tank at site in accordance with manufacturer's instructions and recommendations.
- D. Secure tanks with tie downs at site until installed.

#### PART 2 PRODUCTS

#### 2.01 DESIGN PARAMETERS

A. The storage tanks shall be designed with a vertical configuration with a dish bottom and a flat top. See Sheet 9

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- of 10. The bottom is dished to prevent material bridging during discharge and to improve mixability of any residual solids. The top of the tank is flat to permit easy access to top entering fittings. The top of tank(s) will have a peripheral handrail to protect personnel. The top of the tank will have additional channel stiffeners to support mixer weight and torque.
- B. The tank will be of 5/16-inch wall thickness which will permit up to 1/8-inch for corrosion and erosion allowance. However, the waste solvents and inks being processed would not be expected to be corrosive to carbon steel.
- C. The discharge from the tank(s) will be from the very bottom. The fill point for the tank(s) will be near the bottom of the vertical wall. A check valve will be located in the influent line adjacent to the tank to prevent tank drainage in the unlikely event of pipe failure upstream in the influent line to the storage tank(s).
- D. The outside surface of the tank(s) will be prepped, primed, and finished with an alkyd enamel.
- E. The tank(s) will be provided with a pressure / vacuum vent for normal operation and an emergency bent for abnormal operation. In addition, the unfilled portion of the tank(s) will be blanketed with nitrogen to prevent an explosive atmosphere from existing in the tank(s).
- F. The tank(s) will be provided with a liquid level indicator to monitor tank operation.

#### 2.02 AUXILIARY PIPING

A. The piping to the tank farm will be enclosed in a secondary containment trough. See Sheet 10 of 10. The trough will be suppored with columns at 25-foot centers. The lower portion of the pipe support column will be constructed of reinforced concrete to prevent pipe support damage from a wayward vehicle. The piping and trough will slope towards the tank farm with an integral sump at the tank farm end of the trough. The sump will have a liquid sensor to detect any leak in the process piping.

#### PART 3 EXECUTION

#### 3.01 INSPECTION

A. Perform pre-installation tank tightness testing according to manufacturer's instructions to verify tank integrity prior to

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installation.

B. Verify that dimensions and elevations are as shown on plan sheets prior to placement of tank.

#### 3.02 TANK INSTALLATION

- A. Install tank in strict accordance with manufacturer's written instructions, API Recommended Practice 1615 where applicable, and as indicated on plan sheets. Call to the attention of Architect / Engiener any conflict between manufacturer's recommendations and requirements herein for resolution.
- B. Install tank inventory probe and connect to new console according to manufacturer's written instructions and as required for a properly operating system. Provide all required electrical conduits, circuits, and connections from console to equipment at tank as necessary for proper operation of equipment.

END OF SECTION

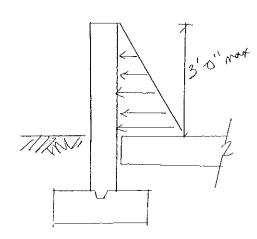
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#### STRESS CALCULATIONS

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ANHALT PROJECT EOG BUIROLMENTAL CHECKED BY:

TANK FARM - CONTAINMENT WACK



WT = 62.4 PSF/ (2.5) = 150PSF/PT FOR 1'-0"WIDE SET. 150 PLF/FT

Mu= 1.7(150RF/4)(3')3=1,2KFf

$$F = bd^{2} = \frac{12(8.5)^{2}}{12000} = 0.072$$

$$K = \frac{M_{u}}{F} = \frac{1.2}{0.72} = \frac{16.61}{1200}$$

Prin = 1.32(0.0013) = 0.0017

Ag= 0.0017(12")(8.5") = 0.17 in /4

#4e 12"OC. Agum AST = 0.2m2/4 (VERTICAL)

mm wall reinforcement.

Ver. p=0.0012

Very = 0.0012(12") = .173112 Hour = 0.002(12)(12) = 0.288 11/4

WITH 2 FRES SF STEEL USE #40 (2) o.c.

1(12m2/FT) = 0,Am2/FT

10/F. #40 12" DIC. FD. MAY - EN EN =

GRAEF ANHALT SOHIDEMER PROJECT EOG ENVIRONMENTAL CHECKED BY:	DATE: 3 · 23 - 95	SHEET
	FRELIMINA	t 10fz
DEFERMINE UNIFORM LOAD UNDER JAN	KS	
FULL TANK WEIGHT MATERIAL STORED SPELFIC GRANITY = 1	7.5	
12000 gallons = 1605ft3		
W= 62.4 PC × 2.5× 1605ft3 = 250K +5	TO FOR TANK WIT	
250X+12,5K= 262.5K		
USE 280K/TANK		
BACH TANK HAS 4 POSTS 280K =	70K/POST	
FOR ENTIRE MAT SLAB THERE IS A 30'x 30' & DIS	TRIBUTION AREA	
4 PANKS × 280K/ANK = 1120K		
1120K = 1.244 kgF = 1244 psf UNIFORM 30'x30=	LOKOING	
ASSUMED ALLOWARDE BEARING PRESSURE =	= 1500P8F Completion of A	zoics p <del>a</del> s
DEPERMINE FREUMINARY SLAB THICKNESS CHECK 2-WAY SHEAR)		
FL=3000psi 21x21 PAD Assume h=16"	d.16"-3"-12"=1	7.5"
Vc=(2+ 4) VFC bod B= = = 1.0 b=1	(4)(2'+12.5')= [46"	
Vc = 4 V 3000 (146" × 12.5") = 400 K		
QVc=.85(400K)=340K Auguarie.		
FOR VU! ASSUME S'XS TUB AREA FOR PAO		
$V_{u} = 1.244 \text{ kg}(1.7)(5' \times 5') - [2' + 12']$ $V_{u} = 1.244 \text{ kg}(1.7)(5' \times 5') - [2' + 12']$ $V_{u} = 70 \text{ k}(1.7) = 119 \text{ k}$	55][] = 33.3K bV_>V_ OK W	8E 110"

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Sheet 2012

TANK FARM MAT FOUNDATION DESIGN (CONT)

PREUMINARY

DETERMINE PRINT, IN MAY SLAB

USE 50" LONG × 1-0" WICE STEEP

M= 1.244ks= (1')(5)31.7) = 26.44 K FT/FT

d=12.5' b=12"

 $F = bd^2 = \frac{12(12.5)^2}{12000} = 0.156$ 

K = 26.44 = 169.5 => 170

P= 0.0030

Ast = 0.003(12)(125)= 0.45 in /ft

USE #60 12" O.C. Agua = 0.44 vin 2/4

USE #60 1240.C EA.WAT TOPE BOTTOM

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#### STRUCTURAL AND STRESS CALCULATIONS

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# [LAB PACK STORAGE TANKS DESIGN]

Acid Storage TOAK - 5500 GAL Cousting Storage TOAK - 5500 GAL

$$\phi = 8ft$$

$$A = Mr^{2}$$

$$= 7(4)^{2}$$

$$= 50.24ft^{3}$$

$$V_{ff} = 50.24 ft^2 \times \frac{7.48 gel}{ft^3}$$
  
= 375.8 gel / ft

Required Height

= 14,64 ft

Assume Dish Depth of 1/2 St

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- (P) Pressure at bottom of vessel

  Assume specific gravity = 2.0

  Vessel & = 8 ft

  Vessel Straight Well = 14 ft

  Depth of Dish = 1/2 ft

  P = (14 + 1.5') (2.0) (62.4 16s/543)

  = 1934 16s/ft<sup>2</sup>

  = 13.4 psi
- Per Pressure Vessel Handbook by Eugene Magyesy
  Assume
  - (E) joint efficiency 20.70
  - (s) design stress = 17,500 psi
  - (P) design pressure = 13.4ps;
  - (R) tank radius = 48 inches
  - (L) dish are radius = 96 inches

			e.
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for Cylindrical Shell (Long Seam)

twell thickness required  $\frac{PR}{SE + 0.4P}$   $\frac{2(13.4)(48)}{(17,500)(0.70) + 0.4(13.4)}$  = 0.052 inches

For Torispherical Head

when  $L/r = 16^{3}/3$ twell thickness required = 0.885 PL = 0.885 (13.4)(96)

17,500 (0.70) + 0.8 (13.4) = 0.093 inches

... for 1/4" thick tank dish

0.25"-0.093"

= 0.157 inches of material

available for erosion or

corrossion in the event of lining failure

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# LAB PACK STORAGE TANK CONCRETE DESIGN

5500 GAL ACID & CAUSTIC TANKS

Full Tank Weight

Max Specific Growing = 2.0

W = 5500 GAL X 8.3416 X J.O

= 91740 lbs

4600 165 5% Tank WA Allowance
96,340 165

Each Took has 4 Legs

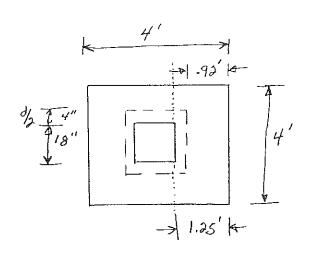
 $W+ per Leg = \frac{96,340 lbs}{4}$ = 24,085 lbs

Assume Allowable Bearing Capacity of 1500 psf

Required Footprint Per Leg

 $A = \frac{\omega}{1500 psf}$   $= \frac{24,085 lks}{1500 psf}$   $= 16.05 ft^{2}$ Assume 4'x4' Footprint

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Assume

Concrete thickness = 9"

No 5 rebar @ 18"c-C

rebar @ 5" from top

Concrete strength 3500ps.

Bending Moment in Slab Adjacent to Proof Plate

M = (1500 psf)(1.85 p)(45+)(1.25/2 f1)

= 4687 pt-#

MuH = 4687 for# x 1,7 (seferty factor)
= 7968 ft -#

Rebar provided  $P = \frac{As}{bd}$   $= \frac{(0.31in^2)(4)}{(48in)(5in)}$  = 0.005

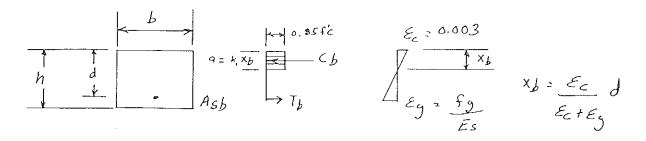
0.005 L 0.027 (.75Pg) OK See Sheet 3

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GRAEF ANHALT SCHLOEMER	PROJECT	E0G	Lab Park	CHECKED BY:	DATE:	3/5

### Concrete Design - Ultimate Strength Method

Given f'c = 3500 psi fy = 60,000 psi K,=0.85 if f'e & 400 psi



Balance Ratio 
$$P_b = \frac{0.85 \text{ fc k.}}{\text{fg}} \left( \frac{87,000}{87,000 + \text{fg}} \right)$$

$$= \frac{0.85 (3500)(0.85)}{40,000} \left( \frac{87,000}{87,000 + 60,000} \right)$$

$$= 0.037$$

ACI code limits tension reinforcement to 75% of the balanced ratio

$$-75 P_b = (.75)(0.037)$$
$$= 0.027$$

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Ultimate Strength Available

$$T = As \frac{sy}{2}$$

$$= \frac{0.31ih^2}{4t} \times 4st \times 60,000psi$$

$$= 74,400 lbs$$

$$= \frac{74,400 \text{ lbs}}{0.85(350\text{ps:})(48:n)}$$
$$= 0.52$$

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SIDEWALL AND BOTTOM STRUCTURE AND CORROSION CALCULATIO					
	SIDEWALL AN	D BOTTOM STRUC	CTURE AND CORR	OSION CALCUL	ATION

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| for Cylindrical Shell (Long Sean) |

twall thickness required =  $\frac{PR}{SE + 0.4 P}$ =  $\frac{(13.9)(72)}{(17,500)(0.70) + 0.4(13.9)}$ = 0.082 inches

for Tovispherical Head  $\int$  when  $4/r = 16^{2/3}$ 

t = 0.885 P L SE + 0.8 P

> = 0.885 (13.9)(144) (17,500)(0.70) + 0.8(13.9)

= 0.145 inches

.. for 1/4" thick tank well
0.25" - 0.145"

2 0.105 inches of material available for erosion or corrossion

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	Engineers & Scientists	PROJECT NO.	95791	<b>/</b> 0 BY: _	GJR	DATE:	10-30-95	SHE	ET
GRAEF ANHALT SCHLOEMER	PROJECT	506		CHECKED BY: _	WPF	DATE:	11/1/95		/ 2

# Storage Vessel Design - TANK FARM

(P) Pressure at bottom of vessel

Assume specific gravity = 2.0

Vessel \$\phi = 12 \text{ ft}\$

Vessel straight wall = 14 \text{ ft}

Height of Dish = 2 \text{ ft}

P= (a,0) (14 'ta') (62.4 |bs/\text{ ft}^3)

= 1996 |bs/\text{ ft}^2

= 13.9 \text{ psi}

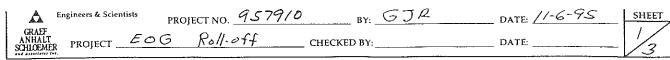
Per Pressure Vessel Handbook by Eugene Megyesg
Assume

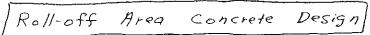
- (E) joint efficiency = 0.70
- (5) design stress = 17,500 psi
- (p) design pressure = 13.9 psi
- (R) tank radius = 72 inches
- (L) dish are radius 2 144 inches

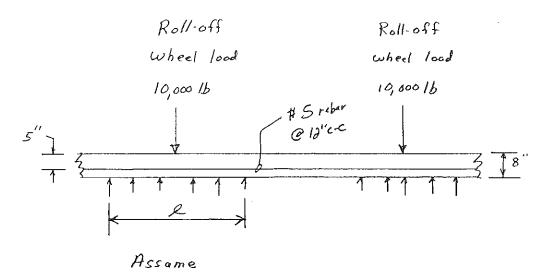
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#### STRUCTURAL LOADING CALCULATIONS

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max Rolloff wheel load = 10,000 16

Concrete thickness = 8 inch

No 5 rebar @ 13" C-C (0.31:n²)

Soil pressure capability = 1500 psf

Loading carried by 2 ft wide Strip

10,000 | bs = 
$$3 + (1)(1500 psf)$$

L reg'd =  $3.33 + f$ 

Max moment below wheel

 $M = (1500 psf)(3ff)(\frac{3.33ff}{2})(\frac{3.33ff}{4})$ 

=  $4158 + f + \#$ 

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GRAEF ANHALT SCHLOEME	R PROJECT EOG	Roll off	CHECKED BY:	DATE:	2/3

# Concrete Design - Ultimate Strength Method

Given f'c = 3500 psi fg = 60,000 psi K,=0.85 if f'c & 400 psi

Balance Ratio 
$$P_{b} = \frac{0.85 \text{ fc}}{\text{fg}} \frac{\text{k}}{87,000} \frac{(87,000)}{87,000 + \text{fg}}$$

$$= \frac{0.85 (3500)(0.85)}{40,000} \frac{(87,000)}{87,000 + 60,000}$$

$$= 0.037$$

ACI code limits tension reinforcement to 75% of the balanced ratio

$$-75 P_b = (.75) (0.037)$$
$$= 0.027$$

*	``	v	

Rebar provided
$$P = \frac{As}{bd}$$

$$= \frac{(0.31)(2)}{(24)(5)}$$

$$= 0.005$$

$$\begin{array}{r} a = \frac{7}{0.85} \frac{7}{56} b \\ = \frac{37,200}{0.85(3500)(24)} \\ = 0.52 \end{array}$$

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#### ATTACHMENT 17: PHASED CONSTRUCTION REVISIONS



JG Disposal, Inc.

February 22, 1996

(414) 353-1156 • Fax (414) 353-1822

(800) 234-1156

Mr. Pat Brady Wisconsin Department of Natural Resources 4041 North Richards Street P.O. Box 12436 Milwaukee, Wisconsin 53212

Feasibility Study and Plan of Operation Report RE:

EOG Disposal, Inc. 5611 West Hemlock Street, Milwaukee, WI

EPA ID# WID988580056

Dear Mr. Brady,

Thank you for meeting with us regarding the changes we are requesting to make to the Feasibility Study/Plan of Operation Report (FPOR) submitted to the Wisconsin Department of Natural Resources on September 6, 1994. The following is a description of the additional operations we propose to implement before completion of the Phase II retrofit and completion of Phase IV.

These changes are to include a lab pack re-packaging and drum transfer/storage operation in the existing EOG Disposal, Inc. building during the Phase II Retrofit. The lab pack re-packaging operations will allow EOG the capability of re-packaging compatible laboratory chemicals from small containers into larger containers for off-site shipment to permitted Treatment Storage and Disposal Facilities. The transfer/storage operation will allow EOG to store drummed materials until truck load quantities can be sent off-site for Treatment or Recycling. These operations will take place during the Phase II Retrofit and will continue until the Lab pack Depack building is constructed and is operational.

EOG is committed to completing the construction of our hazardous waste management facility as outlined in the FPOR. The overall construction time table will depend on weather conditions and department approvals. The Lab Pack Depack building will be started as soon as the site preparation is completed so that the lab pack re-packaging operations can be moved into the new building. If conditions permit, Phase IV will be constructed in conjunction with Phase V.

The following is a revised construction schedule:

Phase I:

Retrofit of the existing building that will include replacement of permeable curbing, installation of a surveillance and alarm system and sealing of floors for acceptance of all wastes with the exception of ignitables. This retrofit will begin March 15, 1996 and is expected to take 2 weeks.

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Phase II: Remaining Retrofit of the existing building. Construction is

expected to take 3 months.

Phase III: Site preparation will begin April 1, 1996 and is expected to take

4-5 months.

Phase IV: Construction of the Lab Pack Depack building will begin September

1, 1996 and is expected to take 4-5 months.

Phase V: Construction of the tank farm and roll-off container storage area

will begin September 1, 1996 and is expected to take 4 months to

construct.

Phase VI: Addition to the existing EOG Disposal building. Construction

timetable has not been determined.

EOG will seek licensing for container storage after Phase I construction and a modification to this license for acceptance of ignitables after Phase II construction. License applications for the remaining phases will depend on construction completion dates. EOG will combine license applications when possible. For example, if the tank farm is completed at the same time as the Lab Pack Depack building, EOG will submit one tank license application for the tanks in the Lab Pack Depack Building and the tank farm.

EOG will be accepting Toxicity Characteristic wastes, hazardous wastes from non-specific sources, hazardous wastes from specific sources, various discarded commercial chemical products, off-specification materials, container residues, spill residues and various laboratory chemicals generated by EOG's existing and future clients. EOG will not accept any ignitable materials until the Phase II Retrofit has been completed.

The layout of the proposed lab pack storage and repackaging areas is illustrated in the attached Figure 1. EOG will set up five separate storage and repack areas that will have distinct boundaries and will be marked with yellow painted lines. The hazard class of the material in each storage/repack area will be clearly communicated by hazardous materials placards corresponding to the materials that are presently in that storage/repack area. The storage areas will be located on both the north side and the southwest corner of existing EOG Disposal building. In each storage/repack area the drums will be placed on spill containment pallets which will elevate the drums 6.5 inches off the floor and will provide enough room to hold either six or eight 55 gallon drums on its surface. The secondary containment capacity for the eight drum pallets is 82 gallons. The secondary containment capacity for the six drum pallets is 61 gallons.

As lab packs are received in 5, 10, 20 and 30 gallon containers they will be placed in appropriately designated storage/repack areas. They will then be depacked and repackaged in

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to larger containers. All depacking will be done on top of the containment pallets. Containers in the lab packs will be combined with other containers in the lab packs without opening any of the containers. The contents of the containers in the lab packs will not be combined with any of the containers.

Bulk drummed materials received will be placed in appropriately designated storage areas to await transfer and shipment to permitted TSDFs.

The proposed operations will allow for storage of up to 468 hazardous waste containers and 280 non-hazardous waste containers or any combination of the above.

STORAGE/REPACK AREA 1: Is located along the north wall of the facility and measures 40 feet by 30 feet. It has enough area for 20 spill containment pallets (10 x 6 drum pallets and 10 x 8 drum pallets) holding a maximum of 140 x 55 gallon drums of material. This area will be used primarily for the storage and repackaging of hazard class 9 (other regulated materials) containers. The secondary containment for this storage area is 1,430 gallons.

STORAGE/REPACK AREA 2: Is located along the north wall adjacent to area 1 and measures 15 feet by 30 feet. It has enough area for 8 spill containment pallets (4 x 8 drum pallets and 4 x 6 drum pallets) holding a maximum of 56 x 55 gallon drums of material. This area will be used primarily for the storage and repackaging of reactive containers. The secondary containment for this area is 572 gallons.

STORAGE/REPACK AREA 3: Is located along the south wall of the facility opposite area 1 and measures 18 feet by 30 feet. It has enough area for 8 spill containment pallets ( $4 \times 8$  drum pallets and  $4 \times 6$  drum pallets) holding a maximum of  $56 \times 55$  gallon drums of material. This area will be used primarily for the storage and repackaging of corrosive bases (pH > 12.5) containers. The secondary containment for this area is 572 gallons.

STORAGE/REPACK AREA 4: Is located along the south wall of the facility and to the west adjacent to area 3. It measures 30 feet by 30 feet and has enough area for 16 spill containment pallets (8 x 8 drum pallets and 8 x 6 drum pallets) holding a maximum of 112 x 55 gallon drums of material. It will be used primarily for the storage and repackaging of poison containers. The secondary containment for this area is 1,144 gallons.

STORAGE/REPACK AREA 5: Is located in the southwest corner of the facility and measures 15 feet by 72 feet. It has enough area for 14 spill containment pallets (10 x 8 drum pallets and 4 x 6 drum pallets) holding a maximum of 104 x 55 gallon drums of material. It will be used primarily for the storage and repackaging of corrosive acid (pH < 2) containers. The secondary containment for this area is 1,064 gallons.

The above listed capacities all refer to 55 gallon drums. Pallets may actually contain drums of various sizes such as 5, 10, 20 and 30 gallon containers.

Depending on the quantities of various drums received, the hazard classes specified above for Storage/Repack areas may be interchanged. For instance, if EOG Disposal received 75 drums

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of corrosive bases, area 1 may be designated for corrosive base storage and area 3 designated for hazard class 9 storage. Only chemicals that are compatible will be stored in each area. Common incompatibles which will not be stored together include acids with bases, acids with cyanides.

During the day to day operations spills of various materials may occur. The spill containment pallets are designed to prevent spilled materials from spreading throughout the storage/repack areas. In the event of a spill, steps will immediately be taken to clean up the spill and prevent the cross contamination of different wastes. The first step will be to identify the leaking container(s) and to stop the container from leaking the rest of its contents. Next, if there are any other containers on the same pallet as the leaking container they will be moved to another containment pallet in the same storage/repack area. The contents of the leaking drum will then be transferred to a proper container. Any spilled material that was contained in the pallet will also be transferred into this container. The containment pallet will then be decontaminated before it is used again.

The first step in the decontamination process is to soak up any remaining liquids that remain in the spill containment pallet with towels, pigs or other absorbents. The pallet grate and the containment area of the pallet will be washed with a solution of biodegradable degreasing cleaner and water using scrub brushes and rags to physically remove any residue left on the pallet or pallet grate. The pallet grate and the containment area of the pallet will then be triple rinsed with a dilute solution of cleaner and water a total of three times. The resultant contaminated cleaning solution, rinsate, rags and absorbents will be collected into drums and disposed of at a fully permitted TSDF.

After the completion of the Phase II Retrofit and approval of this modification, EOG will be accepting ignitables. Storage Area 1 will be designated as ignitable storage. Precautions taken in the container storage area to prevent accidental fire and explosion include the proper storage of containers (stacking, aisle space, labeling and sealing of containers) dikes and warning signs. Smoking is prohibited. To prevent sources of external ignition, explosion proof electrical equipment will be used in all ignitable liquids storage areas.

Containers holding ignitable waste are stored 50 feet from the property line.

Open flames are prohibited in areas where ignitable wastes are handled.

All containers are compatible to the material stored in them. Incompatible materials are separated and stored in designated areas.

In addition to the storage/repack areas there will also be a supply area for containers, vermiculite and pallets. This will be in the area marked supplies on figure 1. This is the area currently utilized for supply storage and currently ocuppied by the laboratory. The laboratory walls will be taken down and all equipment will be moved into the area marked as the office.

The additional drum storage illustrated on figure 1 will be utilized for non-hazardous drummed materials. Lab packs will only be placed in designated storage areas 1-5.

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It is EOG's policy to manage these wastes in the most cost effective way possible, making sure that no backlog of wastes is stored on-site for extended periods of time.

Completion of the Phase II Retrofit will continue during the lab pack re-packaging and drum transfer/storage operations. Worker safety will be of the utmost importance. Lab Pack repackaging and transfer/storage operations will not take place while construction workers are working on the retrofit.

During the lab pack re-packaging operations, EOG will adhere to all of the relevant procedures described in the Feasibility and Plan of Operation Report (FPOR). The following is a listing of each of the FPOR Attachments and their related procedures:

Prior to acceptance, a Waste Profile Sheet and lab pack drum inventory for lab packs and waste streams will be completed by the generator or broker and forwarded to the Approvals Coordinator for review as described in Attachment 5, WASTE ANALYSIS PLAN, Section 2 of the FPOR.

Waste Streams will be sampled and analyzed per the requirements of Attachment 5, WASTE ANALYSIS PLAN, Section 4. Shipment Screening will be completed per the requirements of Attachment 5, WASTE ANALYSIS PLAN, Section 5. EOG will follow the Sampling Procedures described in Attachment 5, WASTE ANALYSIS PLAN, Section 7.

EOG will follow the Rejection Procedures as described in Attachment 5, WASTE ANALYSIS PLAN, Section 6.

During the lab pack depack and storage/transfer operations appropriate components of the Inspection Schedule, described in Attachment 6, of the FPOR will be phased into normal operating procedures.

EOG will follow the Operation and Maintenance Procedure described in Attachment 7, PROCESS INFORMATION, Section 2.7.

EOG will follow the Aisle Spacing Requirements described in Attachment 8, PREPAREDNESS AND PREVENTION PLAN, Section 5.

EOG will follow the Service Arrangements described in Attachment 8, PREPAREDNESS AND PREVENTION PLAN, Section 6.

Loading and off-loading operations will be followed as described in Attachment 8, PREPAREDNESS AND PREVENTION PLAN, Section 7.

EOG will follow Preventative and Remedial Actions procedures as described in Attachment 8, PREPAREDNESS AND PREVENTION PLAN, Section 8.2 and 8.4.

EOG will follow the Runoff Prevention Procedures described in Attachment 8, PREPAREDNESS AND PREVENTION PLAN, Section 9.1.

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EOG will follow the Employee Exposure Prevention procedures described in Attachment 8, PREPAREDNESS AND PREVENTION PLAN, Section 10.

EOG will follow the Groundwater Contamination Prevention procedures described in Attachment 8, PREPAREDNESS AND PREVENTION PLAN, Section 11.

EOG will follow all of the relevant procedures described in Attachment 8, SPILL PREVENTION CONTROL AND COUNTERMEASURE.

EOG will follow all of the procedures described in Attachment 9, CONTINGENCY PLAN.

EOG will follow all of the relevant procedures described in Attachment 11, CLOSURE PLAN.

Closure costs for the proposed lab pack re-packaging and drum transfer/storage operations are estimated to total \$128,212.70. These costs are illustrated in the attached Table 1 and Table 2. The recycling/disposal costs listed in these tables are based on an inventory of 60% lab packs and 40% hazardous waste drums. When the lab pack re-packaging operations are moved to the Lab Pack Depack building, the spill containment pallets will continue to be used for operations in the existing EOG Disposal building. Any contaminated spill containment pallets will be decontaminated prior to reuse. The decontamination calculation for the spill containment pallets of \$715 shown in Table 1 and Table 2 is based on decontaminating 20% of the 66 pallets at \$55 each.

EOG Disposal currently has an insurance policy for closure in the amount of \$151,503.00 and proposes to continue this policy in its current dollar amount. When Phase IV and Phase V are permitted, the closure amount will be revised to reflect Table 4 in Attachment 11, CLOSURE PLAN, of the FPOR.

We look forward to your comments regarding these proposed changes. If you have any questions regarding this request please contact me.

Sincerely,

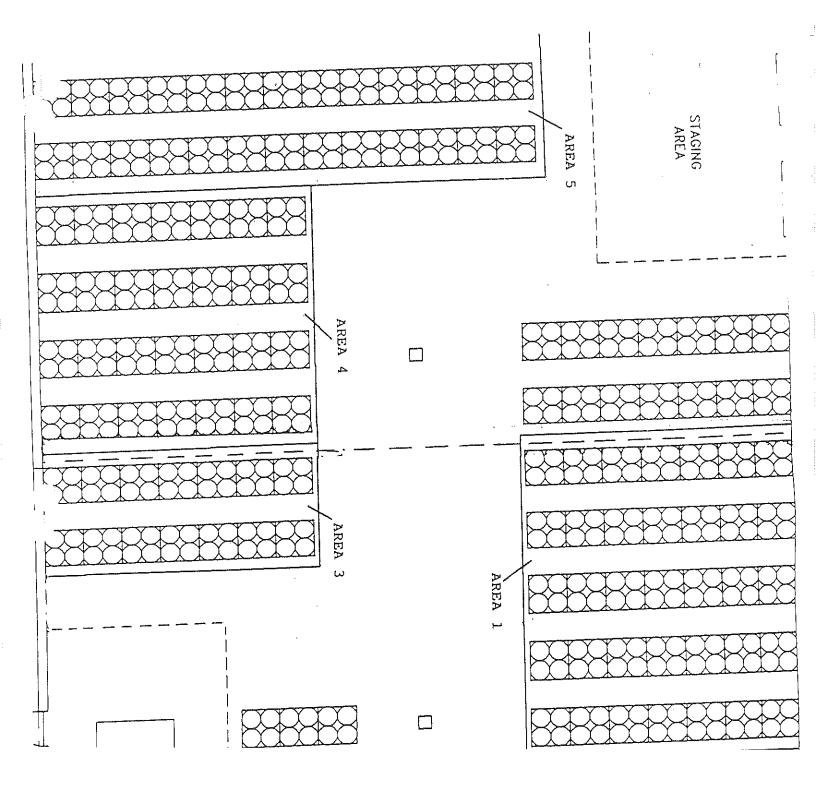
EOG Disposal, Incorporated

Michael C. Vilione, President VK Investments (Owner)

cc: Ed Lynch

Tom McElligott

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TABLE 1
CLOSURE COST ESTIMATE

Closure Activities	Unit Cost	Quantity	Total (\$)
Recycling/Disposal of Hazardous Waste Drum Inventory	non-responsive	187	\$24,310.00
Recycling/Disposal of Lab-Pack Drum Inventory		281	\$56,200.00
Transportation Costs		6	\$1,800.00
Storage Areas -decontaminate floor surfaces -rinsate analyses -decontaminate containment pallets		1 6 13	\$5,250.00 \$6,282.00 \$715.00
Closure-Derived Waste Management - solid residues - liquid residues		2,500 15,000	\$2,500.00 \$7,500.00
Engineering - closure observation - documentation report		5 1	\$6,000.00 \$6,000.00
10% Contingency		1	\$11,584.20
TOTAL		_	\$127,426.20

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TABLE 2 CLOSURE COST ESTIMATE

Closure Activities	Hazardous Waste Storage Closure Cost Estimate <sup>1</sup>	Nonhazardous Waste Storage Closure Cost Estimate <sup>2</sup>
D. Live Disposal of Inventory	\$80,510.00	\$16,600.00
Recycling/Disposal of Inventory  Transportation Costs	\$1,800.00	3
Storage Areas - decontaminate floor surfaces - rinsate analyses -decontaminate spill containment pallets	\$5,250.00 \$6,282.00 \$715.00	NR NR NR
Closure-Derived Waste Management - solid residues - liquid residues	\$2,500.00 \$7,500.00	NR NR
Engineering - closure observation activities	\$6,000.00 \$6,000.00	NR NR
- documentation report	\$11,655.70	\$1,660
10% Contingency TOTAL	\$128,212.70	\$18,260.00

- NOTES: Based on Closure Plan Cost Estimate (see TABLE 1).
- for disposal and transportation costs. Based on non-responsive for dis Included in disposal of inventory unit cost.

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Slab Shear Calculations

2 Way Shear

Vu = Pnet (area) = 1.5 [(4)(4) - (1.08)(1.08)]

= 22.25 Kips

 $V_{4} = \frac{V_{4}}{bd} = \frac{22,250}{4(18+8)(8)}$ = 26 psi

Allowable Nuc = 4 \$ S'C = 4 (0.95) \$\sqrt{3500}\$ = 201 psi 7 26psi OK

I Way Shear

Vu = 1.5 (0.92')(4.0') = 5.52 Kips

 $Nu^{2} \frac{Vu}{bd} = \frac{5,520}{(4)(12)(8)}$ = 14.4 poi

Allow war = 2 \$ Note = 2 (6.85) \$\square\$3500 = 100.5 psi 7/4,4psi OK

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# ATTACHMENT 18: LICENSING CORRESPONDENCE

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NOTICE OF INCOMPLETENESS RESPONSE DATED FEBRUARY 27, 1995

NOTICE OF INCOMPLETENESS RESPONSE DATED APRIL 21, 1995

NOTICE OF COMPLETENESS & PRELIMINARY DETERMINATION RESPONSE DATED NOVEMBER 19, 1995

FEASIBILITY AND PLAN OF OPERATION DETERMINATION DATED APRIL 19, 1996

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Mr. Pat Brady Wisconsin Department of Natural Resources 4041 North Richards Street P.O. Box 12436 Milwaukee, WI 53212

RE:

Feasibility Report and Plan of Operation

Notice of Incompleteness Response for Non-Design Related Issues EOG Disposal, Inc. (EOG) 5611 West Hemlock, Milwaukee, WI

EPA I.D.#: WID 988580056

Dear Mr. Brady,

On behalf of EOG Disposal, Inc., RMT has prepared a response to your letter of incompleteness dated December 9, 1994 for EOG's September 1994 FRPO submittal. Your letter addressed both points of completeness and points of adequacy.

As requested in your letter. EOG has submitted the following information as replacement pages and/or additional pages to the original document. All replacement pages and additional pages have been marked as such and include the date of this response submittal.

This response has been prepared on a point by point basis from the December 9, 1994 Notice of Incompleteness letter for ease of review. As discussed during our January 3, 1995 meeting with you, EOG has responded only to the non-design related issues of incompleteness and inadequacy at this time.

We trust this information is sufficient for your review. We look forward to WDNR's issuance of EOG's operation license.

Sincerely,

RMT, Inc.

Douglas A. Wierman Project Manager

cc:

Mike Vilione Henry Krier Tom McElligott Ed Lynch



RESIDUALS MANAGEMENT TECHNOLOGY, INC. — CHICAGO 999 PLAZA DRIVE - SUITE 100 SCHAUMBURG, IL - 60173-5407

708/995-1500 - 708/995-1900 FAX

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### **GENERAL CONCERNS**

Comment #1: Throughout the FRPO flammable is used interchangeably with ignitable.

The hazardous waste regulations apply to ignitable wastes not flammable wastes. EOG shall change any inappropriate uses of flammable in the

FRPO.

EOG Response #1: EOG has changed all inappropriate uses of flammable in the FRPO.

Attachments 2 through 11 contain the pages of the FRPO have been corrected.

Comment #2: EOG should not reference the federal code unless the state has not

promulgated comparable regulations. EOG shall change any inappropriate

references to the federal code in the FRPO.

EOG has removed all references to the federal code which the state has EOG Response #2:

promulgated comparable regulations in the FRPO. Attachments 2 through 11

contain the pages of the FRPO have been corrected.

Comment #3: EOG shall provide information to answer whether s. 144.44(4R), Wisconsin

Statutes, applies to their facility. In order to determine applicability, EOG shall provide adequate information to demonstrate whether or not this

statute applies.

EOG Response #3: Section 144.44(4r), Wisconsin Statutes refers to noncompliance with plans or

> orders. This does not apply because EOG is in compliance with the terms of their solid waste permit and interim status permit for hazardous waste storage which were approved by the department. In accordance with ss. 144,443, Wisconsin Statutes, EOG has provided proof of financial responsibility

> ensuring the availability of funds to comply with the above mentioned plans to the department. EOG has no interest in any other solid or hazardous waste

facilities in Wisconsin.

Comment #4: EOG shall provide information on the other tenants residing in the Megal

Corporation building.

EOG Response #4; Tenants currently residing in the Megal Corporation building include:

> Design Specialties (Manufacture fireplace doors) 5609 W. Hemlock Street Milwaukee, WI 53223 (414) 353-4339

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ARKO (Dog Training School) 5605 W. Hemlock Street Milwaukee, WI 53223 (414) 353-4768

Comment #5:

EOG speaks of exempt recycling activities and reclamation operations in the FRPO. The department would like to see EOG present specific information on each of these processes. EOG should receive concurrence from the department that their recycling activities are exempt activities and not treatment. (attachment 7, section 1, page 5, paragraph 3)

EOG Response #5:

The blending tank will be constructed in accordance with the requirements of WAC NR 645. Information on the blending tank will be submitted under a separate submittal. EOG will keep track of all waste codes blended by use of a waste code tally sheet (see Attachment 13 of this submittal) and all blended materials will carry all waste codes which were mixed, stored and transported off site (see EOG Response # 24 for further information on waste code tracking). If non-hazardous materials are blended with hazardous materials, the blended material will be managed as a hazardous material.

Comment #6:

If some of the operations at the facility that were thought to be recycling should be actually regulated as treatment, EOG shall update the FRPO to reflect licensed treatment activities. ss. NR 640.06(3), and NR 645.06(3), Wisconsin Administrative Code.

EOG Response #6:

All operations proposed at the EOG facility are strictly recycling operations and no treatment operations will occur.

Comment #7:

EOG shall provide more specific information on the liquification process at the facility including what is liquified.

EOG Response #7:

The "liquification process" refers to the dispersement of viscous materials. For example, a heavy ink will disperse when mixed with a solvent. Viscous materials such as paints, resins and inks will be transferred to one of the fuel blending tanks via a conveyor system. When mixed with the solvent in the tank, the solids will disperse or "liquify".

Comment #8:

EOG shall explain what is done with the solvents recovered from the vapor recovery unit.

EOG Response #8:

EOG will be fuel blending recovered solvents from the vapor recovery unit. The condensed vapor will be pumped to one of the blended fuel storage tanks.

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This information is outlined in the original application in Attachment 7, Section 2.3.2, page 12 of the September 1994 submittal.

Comment #9:

Attachment 7, section 2.5, page 14, references drum pumping stations. EOG shall provide more information on these drum pumping stations, including at a minimum where the drum pumping stations would be located throughout the site and a description of the associated piping.

EOG Response #9:

EOG will utilize air motor or explosion-proof electric motor driven drum pumps within the curbed area containing the fuel blending tank to transfer "water-like" low viscosity liquids into the fuel blending tank. The piping will consist of flexible hose attached directly to the drum pump within the containment area. The flexible hose will be connected to schedule 40 steel pipe for the remaining 5-to-10 feet distance to the fuel blending tank. Text has been revised in Attachment 7, Section 2.5, page 14. Attachment 7 of this submittal contains the revised page.

Comment #10:

EOG shall provide more specific information on the blending tank. This information shall include the types of waste that are blended, (hazardous characteristic waste oils, solvents, listed hazardous waste, etc.), what wastes are blended with what other wastes, what wastes are never blended together, and whether the wastes are shipped off site as hazardous wastes. If hazardous wastes are blended in the tank and the wastes from the tank are sent off site as a hazardous waste, the department would apply the same requirements for a hazardous waste storage tank to the blending tank. If this is the case EOG shall show how the blending tank complies with the requirements for a hazardous waste storage tank and submit the same information that would be required for licensing that tank.

EOG Response #10:

The fuel blending tank proposed to be utilized at the facility is intended to blend hazardous characteristic waste oils and solvents as well as hazardous waste solids with a fuel value of 5,000 BTU per pound. This blending will create a pumpable fuel that will contain solids of not greater than 0.25-inch diameter with a pH range within 2 units and 12.5 units. EOG will not blend reactives, PCB's, oxidizers, strong acids or strong bases with the waste fuel mixture. The blended fuel will be transferred to the storage tanks for off-site shipment. The blending tank will be constructed as a hazardous waste storage tank in accordance with the requirements of WAC NR 645. Information on the blending tank will be submitted under a separate submittal.

Comment #11:

Attachment 7, Section 2.3, page 10, paragraph 4, references, "a suitable blended condition." EOG shall provide a clearer explanation of what is "a suitable blended condition."

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EOG Response #11:

The "suitable blended condition" refers to a mixture of fuel that meets the specifications/requirements of the end user as per their permits and waste analysis plan. EOG has incorporated into the text of Attachment 7, Section 2.2.3, page 10, paragraph 2, the meaning of "a suitable blended condition." The corrected pages which address this issue is contained in Attachment 7 of this submittal.

Comment #12:

EOG shall provide a clearer explanation of the drum auger operation at the site. This information shall at a minimum include; a plan sheet of the auger operation, whether both solid and hazardous waste will be processed in the auger, whether solids from the auger would be treated as a solid or a hazardous waste (attachment 7, section 2.2, page 9), how solids will be transferred from the solids auger (whether the solids will be pumped), and the decision making process used to determine where the solids will be transferred.

EOG Response #12:

Additional text and completed plan sheets showing drum auger operation in greater detail will be submitted by EOG under a separate submittal.

Comment #13:

EOG shall provide more information on containment in all of the loading and unloading areas. This information shall include specifications. EOG shall also explain how dock #2 is designed to contain precipitation. (attachment 7, page 8)

EOG Response #13:

EOG will utilize containment ramps and curbs of concrete with epoxy mortar construction as well as containment trenches. The sentence contained in Attachment 7, Section 2.1.2, page 8, paragraph 1 states 'The dock is constructed of concrete, and is designed to contain any precipitation" is incomplete and should read 'The dock is constructed of concrete, and is designed to contain any potential spillage inside the building from mixing with any precipitation." This would be accomplished by means of the containment ramp to be constructed at the dock entrance. The containment ramps to be constructed at each dock entrance will be constructed of minimum 5,000 PSIG compressive strength concrete doweled into the existing concrete floor by means of #4 rebar spaced on a minimum 24-inch centers. The concrete will be topped by an epoxy grout mixture with a minimum compressive strength of 6,000 PSIG that can be "feathered" to match the existing concrete and provide a smooth transition for the truck traffic over the ramp. The final surface will be the seamless epoxy floor surfacing material to be applied on and contiquous with the floor of the building. Text has been revised in Attachment 7, Section 2.1.2, page 8. Attachment 7 of this submittal contains the revised page.

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#### GENERAL REPORT REQUIREMENTS (ch. NR 680, Wisconsin Administrative Code)

Comment #14: EOG shall submit plan sheets showing site construction and operation

topography. These plans should show how final construction will fit into the existing landscape. This should include cross sections, and

construction specifications which show foundations of the facility structures. s . NR 680.05(1)(c)4.f., Wisconsin Administrative Code.

EOG Response #14: Additional text and completed plan sheets showing site construction and

operation topography will be submitted by EOG under a separate submittal.

Comment #15: EOG shall submit a signed copy of the proposed Part A application. s. NR

680.06(3)(a), Wisconsin Administrative Code.

EOG Response #15: Attachment 1 of this submittal contains a signed copy of the Part A application.

Comment #16: EOG shall submit a Part A application for the existing facility that contains

the even number pages. s. NR 680.06(3)(a), Wisconsin Administrative

Code.

EOG Response #16: Attachment 1 of this submittal contains all pages of the Part A application for

the existing facility.

Comment #17: EOG shall provide a chemical and physical analysis of the hazardous

waste to be handled at the facility. At a minimum, these analyses shall contain all of the information which must be known to store the waste in accordance with chs. NR 600 through 685, Wisconsin Administrative Code.

s. NR 680.06(3)(b), Wisconsin Administrative Code.

EOG Response #17: EOG will conduct analysis of six indicator parameters to determine the

acceptability of waste materials, compatibility, BTU's/pound, chloride content,

water content, pH, and specific gravity.

Comment #18: Attachment 3, appendix E, section 1.1, page 3, refers to the recent

extension of RCRA regulations to now include small quantity generators. EOG shall provide a further explanation of what is meant by that statement.

s. NR 680.06(6), Wisconsin Administrative Code.

EOG Response #18: Most waste management companies do not have the capabilities to handle

small quantities of materials. EOG has specialized in dealing with materials from small quantity generators, we have carved out a "niche" in the industry to manage the 1-5 drum quantities of small quantity generators. The text of

Attachment 3, Appendix E, Section 1.1, page 3 has been changed to clarify this

statement. Attachment 4 of this submittal contains the revised page.

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Comment #19:

EOG shall provide information on any other statutory authority or local, state or federal approvals that apply to the facility. s. NR 680.06(6)(a)2., Wisconsin Administrative Code.

EOG Response #19:

No other statutory authority, local, state or federal approvals apply to EOG.

Comment #20:

EOG Shall provide information on any emissions or discharges associated with preparation and construction of the facility. s. NR 680.06(6)(a)4., Wisconsin Administrative Code.

EOG Response #20:

Emissions related to construction equipment will be controlled as appropriate during preparation and construction activities. EOG will also set up temporary silt fences to prevent sediment runoff during preparation and construction of the facility. EOG has incorporated this text into Attachment 3, Appendix E, Section 2.4. These replacement pages are contained in Attachment 4 of this submittal.

Comment #21:

I could not find information on other anticipate changes with facility development. The checklist points out that the information should be in attachment 3, appendix D, section 6. Even assuming appendix E, (see condition #95), I could not locate the information. EOG shall provide such information or point out where such information is located in the FRPO. s. NR 680.06(6)(a)5., Wisconsin Administrative Code.

EOG Response #21:

No other changes associated with the facilities operations are anticipated other than those stated in this application. EOG has incorporated this text into Attachment 3, Appendix E, Section 2.5. These replacement pages are contained in Attachment 4 of this submittal.

Comment #22:

Attachment 2, section 3, page 2, states, "No other permitted facilities in geographic proximity to EOG would offer the diversity of hazardous waste recycling nor the distribution of service." EOG shall explain what they consider to be in the geographic proximity to EOG. EOG shall also explain in more detail their, "diversity of hazardous waste recycling," and their, "distribution of service." In attachment 2, section 5, page 2, EOG states that their, "service area extends throughout the United States." EOG shall discuss in further detail a breakdown of their service area and how their other branch offices work with the Milwaukee facility. s. NR 680.06(8), Wisconsin Administrative Code.

EOG Response #22:

EOG is a full service waste consulting firm located in Milwaukee, Wisconsin with branch offices in Westmont, Illinois, Minneapolis, Minnesota, Salt lake City, Utah and College Station, Texas. The Milwaukee facility is EOG's only processing facility. Each of these offices has an Account Manager that is responsible for sales within that specific region. These sales offices will be

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directing drums from their clients to EOG's Milwaukee facility for processing. EOG has added text to Attachment 2, Section 3, page 2 to clarify this issue. Attachment 2 of this submittal contain the revised page.

## WASTE ANALYSIS PLAN (ss. NR 680.06(3)(c), AND nr 630.13(1) Wisconsin Administrative Code)

Comment #23:

EOG shall explain the criteria for blending of wastes. EOG shall also explain what will be done to ensure that only compatible wastes are blended. EOG shall present a clearer more concrete description of how incompatible wastes and reactive wastes are determined and separated.

EOG Response #23:

To ensure that only compatible wastes are processed and blended, a composite sample of each inbound waste stream to the EOG facility will be subject to compatibility testing (see Attachment 15 of this submittal). If the material is compatible, it will be deemed acceptable for waste-derived-fuel production. If a waste stream material is deemed incompatible, it will not be processed or blended into a waste-derived-fuel.

Comment #24:

Much of hazardous wastes shipped today can have multiple waste codes. EOG shall explain how wastes received at their site with multiple waste codes will be processed through their system and whether they anticipate any problems will occur. EOG shall explain if any waste codes will be lost through the consolidation or processing of the waste.

EOG Response #24

All materials accepted by EOG will be accompanied by a manifest that will have waste codes listed in sections I and J. These waste codes will be transferred onto a tally sheet (see Attachment 12 of this submittal) as the materials are blended. These tally sheets will accompany outgoing manifests. Waste codes are also listed on the "EOG BULK MATERIALS INVENTORY REPORT" located in Attachment 6, Appendix C. The tally sheets and Bulk Materials Inventory report will be filled out manually and the data will then be entered into our computerized inventory control system. This will enable us to track waste codes for all incoming and outgoing waste streams. No waste codes will be lost in the blending of waste streams and waste codes will be carried through all the way to the end-sites.

Comment #25:

EOG shall explain who fills out a waste profile sheet and whether the form is always completely filled out.

EOG Response #25:

Waste profile sheets are to be filled out by the generator or broker. Waste Profile forms accepted by EOG will include EOG's Waste Profile Sheet (WPS), the generators waste identification form, or one of the waste identification forms used by brokers who represent the generator. The Waste Profile form is always completed; however, if some areas of the form are incomplete when submitted,

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EOG will contact the generator and/or broker to gather the information necessary to fully complete the form. EOG has added text to Attachment 5, Section 2, page 2 to clarify this issue. Attachment 5 of this submittal contain the revised pages.

Comment #26:

EOG shall explain what are the minimum requirements that are required on a generator's or broker's waste identification form.

EOG Response #26:

The waste identification form will at a minimum contain Generator Information, Waste Description, General Characteristics, RCRA Information, Viscosity, Total Suspended Solids, pH, BTU's, Flash Point, Halogens, Hazardous Characteristics and Other Components, Chemical Composition and Metals information. EOG has added text to Attachment 5, Section 2, page 2 to clarify this issue. Attachment 5 of this submittal contain the revised pages.

Comment #27:

EOG explains that, "pre-qualification samples are periodically requested for verification and generators shall be requested to periodically resubmit waste identification forms." EOG shall explain what is meant by "periodically." The department would like to see a consistent system in place.

EOG Response #27:

Annual recertification of each active waste stream by each generator will be required to document any changes in the nature of the waste. This will encompass completion of a Waste Profile Sheet and a sample if changes to the waste stream or process generating the waste stream are apparent.

Comment #28:

EOG's use of the descriptor with the table of the list of wastes to be managed on site looks good. The department would like to see EOG add an additional descriptor which would be whether the waste will be sent offsite for use as a secondary fuel.

EOG Response #28:

A descriptor which indicates which materials will be sent off site for use as a secondary fuel has been added to Attachment 5, page 35 and the contents of this table have been updated. Attachment 5 of this submittal contains Table 1 with the new descriptor added.

Comment #29:

EOG shall clearly define what is involved in the precertification process. (attachment 3, section 4, page 31)

EOG Response #29:

Attachment 5, Section 4, page 36, the first sentence has been changed to read as follows: "Generally, any material that has been approved through the prequalification process, consisting of Waste Profile evaluation and sample analysis if required, is initially acceptable." Attachment 5 of this submittal contains the revised page for this issue.

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Comment #30:

Attachment 3, section 4, page 31, mentions that, "the materials may be analyzed for the following parameters in an onsite laboratory to determine their acceptability based on the schedule presented in Section 8, Analysis Plan." EOG shall explain whether materials will always be analyzed based on the schedule.

EOG Response #30:

EOG will analyze for all the parameters listed in Attachment 5, Section 4, page 36 in an on-site laboratory to determine the acceptability based on the schedule presented in Attachment 5, Section 8. Attachment 5 of this submittal contains the revised page.

Comment #31:

Attachment 3, section 7.3, page 37,mentions, "sampling bulk load solids may be done by taking random samples throughout the load." EOG shall explain whether bulk load solids will always be sampled.

EOG Response #31:

EOG will sample bulk solid loads by taking samples throughout the load to make a representative composite sample. Attachment 5 of this submittal contains the revised page.

Comment #32:

Attachment 3, section 5.1, page 32,talks about the receipt of containerized loads. EOG shall rewrite this section so that it is clear what tests are done, when and where the tests are done, and on what wastes the tests are done. The department needs to know how often the waste is sampled.

EOG Response #32:

Containers from each generators waste stream(s) shall also be randomly chosen for analysis and inspection. A minimum of ten percent of the containers of each generators waste stream(s) shall be sampled and analyzed for compatibility, BTU/pound, chloride, water, specific gravity and pH in the onsite laboratory. This same analysis shall be performed for bulk loads. All incoming wastes are sampled. Attachment 5 of this submittal contains the revised pages.

Comment #33:

Attachment 3, section 5.1, page 32, mentions that, "containers shall also be randomly chosen for analysis and inspection." EOG shall explain more clearly how this choosing of containers is done.

EOG Response #33:

A minimum of ten percent of each generator's waste stream(s) shall be sampled and analyzed in the on-site laboratory. Attachment 5 of this submittal contains the revised pages.

Comment #34:

Attachment 8, Spill Prevention Control and Countermeasures Plan, figure 1, Flow Diagram, page 18, contains a very well done and useful flow chart. The department feels it would be a benefit to also include this flow chart in the waste analysis plan and add the analysis done at each stage for waste

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received from offsite and include the type of analysis.

EOG Response #34:

An updated flow diagram has been prepared to include the analysis done at each stage for waste received from off site as well as the type of analysis performed. This flow chart has been added to the Waste Analysis Plan of the permit application. Attachment 5, Appendix C of this submittal contains the updated flow diagram.

Comment #35:

Attachment 3, section 5.2 and section 5.3, page 33, both mention, "and any other analysis as deemed necessary by management." EOG shall discuss what other analyses would be performed and when would they be deemed necessary.

EOG Response #35:

Additional analysis may be necessary on suspect materials to verify that the parameters of the shipped waste reasonably match the parameters provided on the Waste Profile Sheet (WPS) for that waste. Examples of suspected materials and tests performed for verification include the following:

- Reactive testing on methacrylates
- Odor or viscosity to verify with the WPS
- Additional analysis may be necessary such as ash content for end-site disposal approval.

Comment #36:

EOG shall explain if any analysis is performed on lab packs. EOG shall also explain whether the contents of the lab packs will be emptied and combined with like materials. If EOG plans to combine the contents of the lab packs, the department feels that some type of compatibility testing will need to be performed. (attachment 3, section 5.4, page 34)

EOG Response #36:

The contents of the lab packs will be de-packed. The lab packs will then undergo one of the following:

- consolidated and blended to produce a waste-derived fuel,
- repacked with other compatible chemicals, or;
- consolidated into the acid or basic storage tanks.

Lab packs not suitable for consolidation will be repacked with compatible chemicals. All other lab packs will undergo testing for compatibility once they have been depacked. For lab packs consolidated for fuel blending, the same six parameters identified in EOG Response #30 will be analyzed per composite waste stream.

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Comment #37:

After EOG signs off on the manifest, they are unable to send the waste back to the generator unless the generator is a licensed facility able to receive waste from offsite. EOG shall include a statement in the waste analysis plan that reflects this issue. (attachment 3, section 6, page 35)

EOG Response #37:

If a full load of material is rejected, the manifest will not be signed by EOG. If a partial load of containerized material is rejected, the containers will be noted in section 19 of the manifest and then the manifest will be signed by EOG to certify receipt of non-rejected containers. Text has been inserted in Attachment 5, Section 6, page 40 to clarify this issue. Attachment 5 of this submittal contains the revised page.

Comment #38:

EOG shall explain how they could reject only a part of a bulk load. (attachment 3, section 6.2, page 5)

EOG Response #38:

EOG expects that bulk waste may be delivered in compartmentalized trailers. In this case EOG can reject a part of a bulk load. Text has been added to Attachment 5, Section 6.2, page 5 to clarify this issue. Attachment 5 of this submittal contains the revised page.

Comment # 39:

Attachment 3, section 6.4, page 36, concerns the rejection procedures for polychlorinated biphenyl loads. If PCB's are received at the site in units other than lab packs, EOG shall change the wording to reflect the use of other units.

EOG Response #39:

EOG has changed the wording of Attachment 5, Section 6.4, page 41, sentence 1 to reflect PCB's being received at the site in units (i.e., capacitors, ballasts, etc.) other than lab packs. Attachment 5 of this submittal contains the revised page.

Comment #40:

EOG shall explain what products are produced at the facility. (attachment 3, section 11, page 61)

EOG Response #40

Products produced at the EOG facility will consist of "usable fuel products". EOG has changed the wording in Attachment 5, Section 11, page 66 to better describe the products produced at EOG's facility. Attachment 5 of this submittal contains the revised page.

Comment #41:

In attachment 3, table 2, pages 39 through 58, EOG shall list what are each of the "other" tests.

EOG Response #41:

EOG has revised Table 2 of Attachment 5 to include the analysis performed for all wastes having waste codes received at EOG. Attachment 5 of this submittal contains the revised Table 2.

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Comment #42:

EOG shall explain whether the analyses listed in attachment 3, table 2, pages 39 through 58 are the only analyses performed on the waste and

when these analyses would be performed on the waste.

The analysis listed on revised Table 2 of Attachment 5 will be completed on EOG Response #42:

each waste stream when it arrives at the EOG facility.

EOG shall explain who will be performing the waste analysis. Comment #43:

Once samples are collected and labeled, they will be brought to the on-site EOG Response #43:

> laboratory for analysis which will be completed by the Laboratory Chemist. Attachment 5, Section 7.1, page 42 has been changed to clarify this issue.

Attachment 5 of this submittal contains the revised page.

EOG shall state that the chemical and physical samples will be analyzed by Comment #44:

a laboratory certified or registered under ch. NR 149. Wisconsin

Administrative Code, as required by ss. NR 630.13(2) and (4), Wisconsin

Administrative Code.

Chemical and physical samples will be analyzed for waste characterization by a EOG Response #44:

laboratory certified or registered under ch. 149, Wisconsin Administrative Code.

Section 4 of Attachment 5 contains the revised page.

CONTAINER REQUIREMENTS (ch. NR 640, Wisconsin Administrative Code. Tank Requirements, (ch. NR 645, Wisconsin Administrative Code), included if they also apply)

Comment #45: The FRPO mentions "these drawings" in attachment 7, section 2.4, page

13, paragraph 4. EOG shall provide more specific information on what

"these drawings" are and where they are located.

Attachment 7, Section 2.4, page 13, text has been revised to indicate that EOG Response #45:

> Sheets 9, 10 and 11 of Attachment 15 depict the typical locations of containers within the storage/process building for storage of up to 2,272 containers,

> however, the number of containers in any of these areas may vary. Attachment

7 of this submittal contains the revised page.

I understand EOG is located on two separately owned properties. EOG Comment #46:

> shall clearly explain the division of the two properties, clearly identify the two property owners, explain how this division of the two properties will be handled for the operation of this site, and explain what problems would be

anticipated in having two separate property owners and how those problems would be addressed. EOG shall explain how the second property owner will be kept informed of activities going on at the site. ss.

NR 640.06(1)(a)2., and 645.06(1)(a)2., Wisconsin Administrative Code.

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EOG Response #46:

EOG has added the new lease agreement between EOG and Megal Development Corp as Appendix F to Attachment 3. EOG has purchased the property and has entered a lease agreement with Megal Development Corp. for office space adjacent to the property. Attachment 16 of this submittal contains the lease agreement.

Comment #47:

EOG shall include in the FRPO whether any parks, hospitals, or nursing homes are within a 1/2 mile radius of the facility. s. NR 640.06(1)(a)3., Wisconsin Administrative Code.

EOG Response #47:

No nursing homes or hospitals are located within a 1/2 mile radius of the EOG facility. There are two country clubs; to the west, approximately 810 feet from the EOG facility is Brynwood Country Club and to the east, approximately 1350 feet from the EOG facility is Tripoli Golf Club no other parks or recreational areas are known to exist within a 1/2 mile radius of the EOG facility. Sheet 6 of 18 of the September 1994 FRPO submittal shows the location of these country clubs in relation to the EOG facility. Text has been added to Attachment 3, Section 2.2, to satisfy WAC NR 640.06(1)(a)3. Attachment 3 of this submittal contains the revised pages.

Comment #48:

EOG lists facilities from all over the country from which they would be accepting waste. EOG shall explain whether these wastes would be going to the Milwaukee site or one of their other sites. ss. NR 640.06(1)(a)4., and NR 645.06(1)(a)4., Wisconsin Administrative Code.

EOG Response #48:

As noted in EOG Response #22, EOG is a full service waste consulting firm located in Milwaukee, Wisconsin with branch offices in Westmont, Illinois, Minneapolis, Minnesota, Salt lake City, Utah and College Station, Texas. The Milwaukee facility is EOG's only processing facility. Each of these offices has an Account Manager that is responsible for sales within that specific region. These sales offices will be directing drums from their clients to EOG's Milwaukee facility for processing. EOG has added text to Attachment 2, Section 3, page 2 to clarify this issue. Attachment 2 of this submittal contains the revised page.

Comment #49:

EOG shall provide a response to the material balance informational request of ss. NR 640.06(1)(a)5. and 7., and NR 645.06(1)(a)5. and 7., Wisconsin Administrative Code, or explain where this information is located in the FRPO. I could not locate this information in attachment 3, section 7.

EOG Response #49:

No wastes will be generated at EOG,s facility. Waste accepted at EOG's facility will be bulked and/or blended for use in secondary markets (i.e., cement kilns) Examples of material balance at this facility are as follows:

## Scenario 1

EOG receives a lab pack containing the following chemicals:

Sulfuric Acid	1 pint	D002
Phosphoric Acid	1/2 gallon	D002
Hydrochloric Acid	1 quart	D002
Nitric Acid Solution 40 %	1 quart	D002
Chromic Acid Solution	4 oz.	D002, D007
Hydrofluoric Acid	1 pint	D002

All of these items will be depacked and consolidated into the acid tank. Any items that are received in a lab pack that could not be bulked would be repacked and sent to an off-site disposal facility for disposal. The containers would be triple rinsed with the rinse water going into the acid tank. The glass jars would then be crushed and sent to a glass reclaimer.

## Scenario 2

EOG receives 55-gallon drums of acetone from an industrial client which carries the EPA waste codes D001 and F003. These drums are pumped into one of the bulk fuel tanks. When the materials from this tank ships off-site, the manifest will carry the D001 and F003 codes as well as any other codes from material bulked into this tank. The RCRA empty drums will be sent off-site to a drum reclaimer.

## Scenario 3

EOG receives a lab pack containing the following chemicals:

Acetone	1 pint	D001, F003
Hexane	1 quart	D001, F005
Toluene	1 pint	D001, F005
Aliyi Alcohol	2x1 pint	D001, P005
Hexachlorobenzene	1/2 pound	U127, D032
Methylene Chloride	1 quart	F002
Phenol	1 pound	U188
Methyl Ethyl Ketone	1/2 gallon	D001, F005, D035
Methanol	2x1 quart	D001, F003
Pyridine	1 pint	D001, F003, D038

All of these items will be depacked and consolidated for fuel. All of the waste codes will be retained through the bulking process. When the materials ship off-site, the manifest will carry all waste codes. The containers would be triple rinsed with the rinse water going into the fuel. The glass jars would then be crushed and sent to a glass reclaimer. Attachment 3, Section 7.1 contains the revised page(s).

Comment #50:

17. The area north of the Megal Corporation building is where traffic will enter the site and access to the site will be controlled. EOG shall provide a clearer description of the area north of the Megal Corporation building. ss. NR 640.06(1)(a)6., NR 640.06(1)(c)6., NR 645.06(1)(a)6., and NR 645.06(1)(c)6., Wisconsin Administrative Code. EOG shall also explain where trucks will be parked when they are waiting to enter the EOG property while multiple loads are being delivered to EOG. ss. NR 640.06(1)(h)4., and NR 645.06(1)(h)4., Wisconsin Administrative Code.

EOG Response #50:

For the expanded facility, waste delivery trucks enter the facility through the main gate located north (rear) of the leased office space. The area north of the lease office space is a paved roadway and parking area. This parking lot area is rarely used by the tenants of the building because sufficient parking space is available in the front of the building. Trucks waiting to enter the facility while multiple loads are being delivered, will park along the northern boundary of the paved roadway. Text has been added to Attachment 3, Section 5. Attachment 3 of this submittal contains the revised page.

Comment #51:

EOG shall identify the persons or person responsible for plant construction. ss. NR 640.06(1)(a)8., and NR 645.06(1)(a)8., Wisconsin Administrative Code.

EOG Response #51:

Henry Krier of EOG will be the primary person responsible for site construction. Megal Corporation will also be involved with the site construction activities. Text has been added to Attachment 3, Section 8 to clarify this issue. Attachment 3 of this submittal contains the revised page.

Comment #52:

EOG shall explain whether an air management permit will be needed for the site. EOG shall present more specific information on air emissions than what is in attachment 3, Section 10.1. ss. NR 640.06(1)(a)9., and NR 645.06(1)(a)9., Wisconsin Administrative Code.

EOG Response #52:

Text has been added to Section 10.1 of Attachment 3. EOG requires a construction air permit and an operating air permit for the site. The construction air permit as a new, non part 70 source (minor source) has been prepared. The construction permit has been submitted to the Wisconsin Department of Natural Resources, and copies have been forwarded to you for your use as Exhibit 1 of this submittal.

Comment #53:

EOG shall provide further information on the facility layout including building and structures foundation, sizing of receiving areas, sizing of major processes and processing equipment. ss. NR 640.06(1)(a)12., and NR 645.06(1)(a)12., Wisconsin Administrative Code.

EOG Response #53:

Additional text and completed plan sheets of building and structures

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foundations, sizing of receiving areas, sizing of major processes and process equipment in greater detail will be submitted by EOG under a separate submittal.

Comment #54:

EOG shall explain the timing of the construction of the new site. EOG explains that the facility will be constructed in a phased approach. The department would like the specifics of the plan because the phased construction might affect the coordination of the licensing at the facility. EOG shall provide a time table for start up and operation of the various units at the site. ss. NR 640.06(1)(a)13., and NR 645.13(1)(a)13., Wisconsin Administrative Code.

EOG Response #54:

EOG will complete their facility construction in the following phases:

Phase I:

Retrofit the existing building at 5611 West Hemlock Street to meet permit requirements for storage of

hazardous wastes.

Phase II:

Construction of the Lab Pack Depack building.

Phase III:

Construction of the tank farm.

All necessary security and safety issues associated with each Phase will be self contained. For example, the facility fence and security system will be constructed during Phase I. The facility construction Phases have been added to Attachment 3, Section 8. Attachment 3 of this submittal contains the revised pages.

Comment #55:

EOG shall explain what provisions will be taken during the construction of the facility to ensure protection of groundwater and surface waters. ss. NR 640.06(1)(a)15., and NR 645.06(1)(a)15., Wisconsin Administrative Code.

EOG Response #55:

Additional text and completed plan sheets explaining the provisions that will be taken during construction will be submitted by EOG under a separate submittal.

Comment #56:

In addition to identifying the surrounding businesses, EOG shall identify the surrounding property owners., ss. NR 640.06(1)(b)7., and NR 645.06(1)(b)7., Wisconsin Administrative Code.

EOG Response #56:

The surrounding property owners consist of the following:

5606 W. Hemlock Street (north)
 Megal Development Corp.
 P.O. Box 18661
 Milwaukee, WI 53218